

BUILDINGWORK

PCLS Lakewood Interim Library

SITE BID SET – ADDENDUM NUMBER 3

ISSUED: August 21, 2023

This Addendum supersedes and supplements all portions of the Site Bid Set dated August 4, 2023, with which it concerns. The Addendum becomes part of the Contract Documents upon issuance. Receipt of the addendum must be acknowledged on bid for bid to be considered valid.

This Addendum includes the following Sections and Attachments:

<u>Section 1:</u> Bid Document Clarifications, Revisions, and Additions <u>Section 2:</u> Bidder Questions <u>Attachments:</u> Geotechnical Report, Redlined C103, Revised Specification Sections 015700, 329113

SECTION 1: Bid Document Clarifications, Revisions, and Additions

Revision: City of Lakewood is requiring full replacement of existing asphalt sidewalk on Gravelly Lake Road with Concrete per WSDOT standards. Existing concrete curb and street trees to remain. Construction to be per WSDOT standards. See redlines on Sheet C103 for extent of scope.

Addition: City of Lakewood is requiring the selected contractor to create and submit an SWPPP prior to start of construction. See revised specification section 015700 for requirements.

SECTION 2: Bidder Questions

Question: Plan Sheet C101, Note 10 mentions construction surveying, but the specifications are silent on survey/construction staking outside of quantity verification for unit price work (not applicable.) Please advise if construction staking is owner-provided or if we need to include construction staking costs in our bid.

Answer: Construction staking should be included in contractor costs. Owner will not provide construction staking.



Question: Plan Sheet C101, Note 13 mentions the possibility of needing an NPDES permit and to contact Ecology for information. The specifications are silent on any contractor obligation related to an NPDES permit, and on a project with this short of a timeline and quick anticipated start, we'd expect that the NPDES has been obtained and no contractor obligation outside of any reporting requirement. Please clarify if this permit will be contractor's responsibility.

Answer: The contractor is required to provide and maintain a Stormwater Pollution Prevention Plan (SWPPP) but no additional permitting with the Department of Ecology will be required.

Question: No geotechnical report was included in the bid documents. If one exists, we request it be published to BXWA.

Answer: Geotechnical Report is attached as part of this addendum.

Question: Project Specifications do not include Div 31 (earthwork) or Div 33 (Utilities), but see that Div 32 (Exterior Improvements) is covered by WSDOT standards. Are we to assume Div's 31 and 32 also following WSDOT standards?

Answer: Yes; WSDOT standard specifications for road, bridge, and municipal construction apply to all work not otherwise specifically described in the project manual specifications.

Question: The plans do not include a detail for the 8x6 water connection. Do we have the option to choose a cut-in tee or a hot-tap?

Answer: Connection to be a live tap per City of Lakewood standards

Question: Section 32 9113 Soil Preparation, section 3.3(C) mentions planting area subgrades to be established 15 inches below finish grade. This would leave room for 12 inches of amended topsoil and 3 inches of bark mulch. On plan sheet L102, detail 4 – Soil Amendment shows planting areas to receive 8 inches of amended topsoil and 3 inches of bark mulch. Please clarify.

Answer: Preparation per drawing notes is required. Specification section has been revised to match and is attached.

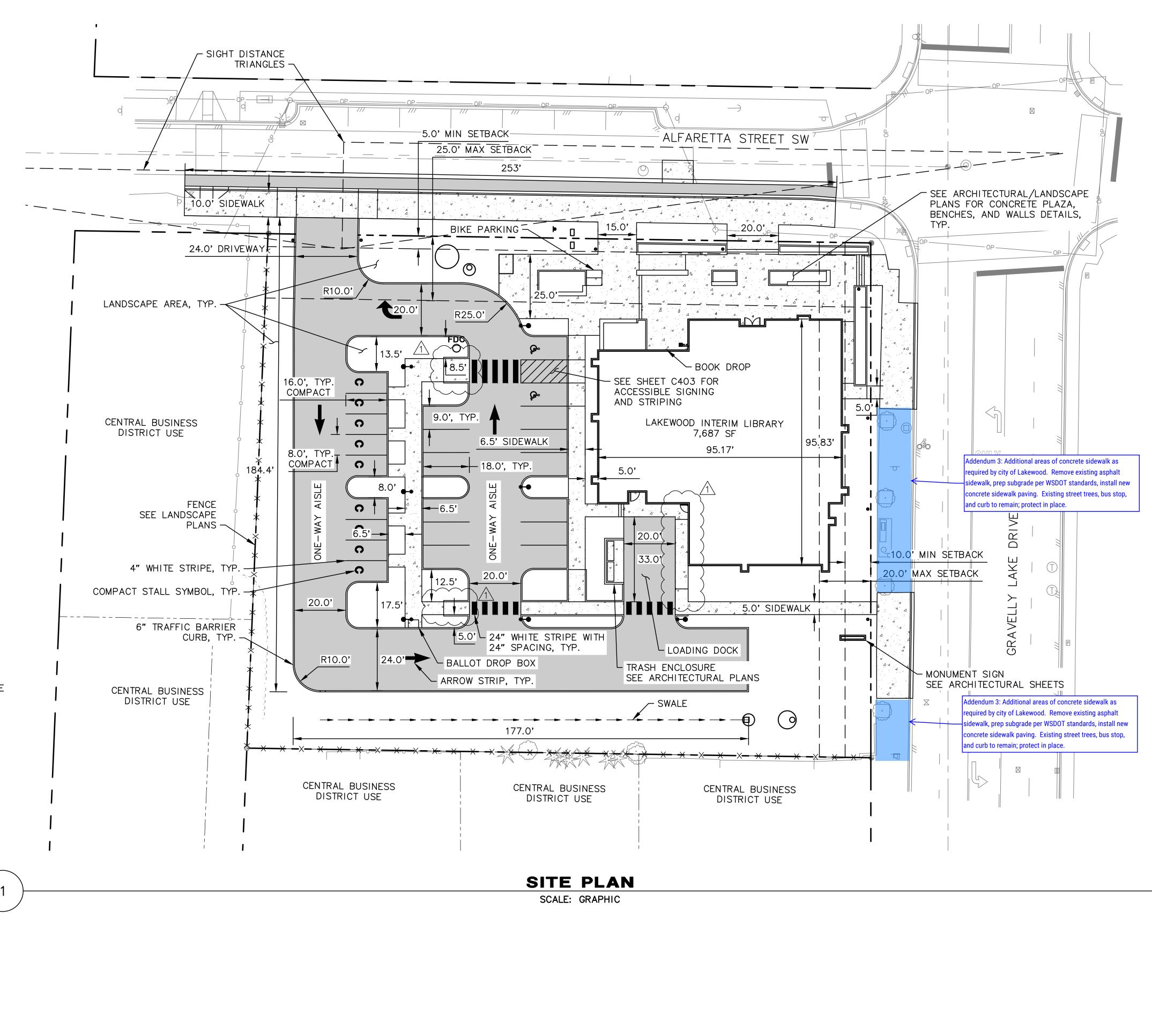
END OF ADDENDUM NUMBER 3

ROADWAY STANDARD NOTES:

- ALL WORK IN CITY RIGHT-OF-WAY REQUIRES A RIGHT-OF-WAY PERMIT FROM THE CITY OF LAKEWOOD. PRIOR TO ANY WORK COMMENCING, THE GENERAL CONTRACTOR SHALL ARRANGE FOR A PRECONSTRUCTION MEETING TO BE ATTENDED BY ALL MAJOR CONTRACTORS, REPRESENTATIVES OF INVOLVED UTILITIES, AND THE CITY OF LAKEWOOD. CONTACT THE CITY OF LAKEWOOD PUBLIC WORKS ENGINEERING DEPARTMENT TO SCHEDULE THE MEETING. THE CONTRACTOR IS RESPONSIBLE TO HAVE THEIR SET OF PLANS AT THE MEETING.
- 2. FOR WORK IN CITY RIGHT-OF-WAY, INSPECTIONS ARE REQUIRED AT THE FOLLOWING CONSTRUCTION STAGES:
- 2.1. INSPECTION NO. 1: CLEARING AND GRUBBING, EMBANKMENT AND EXCAVATION, UNDERGROUND DRAINAGE, WHEN TRENCHING AND PLACEMENT OF PIPE ARE COMPLETE BUT PRIOR TO COVER OR TEMPORARY WATER DETENTION/RETENTION AND SILTATION CONTROL.
- 2.2. INSPECTION NO. 2: GENERAL ROADWAY, WHEN THE DRAINAGE SYSTEM, UNDERGROUND UTILITIES, AND GRADING TO SUITABLE SUBGRADE ARE COMPLETE, INCLUDING GRAVEL BALLAST IF REQUIRED.
- 2.3. INSPECTION NO. 3: GENERAL ROADWAY, WHEN THE CRUSHED GRAVEL SURFACING HAS BEEN PLACED.
- 2.4. INSPECTION NO. 4: GENERAL ROADWAY, WHILE THE PAVING IS IN PROGRESS.
- 2.5. INSPECTION NO. 5: OVERALL ROADWAY, AFTER PAVING, CLEANING OF DRAINAGE SYSTEM AND ALL NECESSARY CLEANUP, STRIPING, BUTTONING, MONUMENTS, AND ALL DELINEATION WORK.
- 3. MONUMENTS SHALL BE INSTALLED AT ALL STREET INTERSECTIONS, AT ANGLE POINTS, AND POINTS OF CURVATURE IN EACH STREET. ALL BOUNDARY MONUMENTS.
- 4. SIGNAGE AND TRAFFIC CONTROL DEVICES ARE SAFETY ITEMS AND SHALL BE INSTALLED PRIOR TO ISSUANCE OF ANY CERTIFICATE OF OCCUPANCY. ALL SIGNAGE SHALL BE IN ACCORDANCE WITH THE MUTCD.
- 5. SIDEWALKS, DRIVEWAYS, AND OTHER IMPROVEMENTS IDENTIFIED IN THE PRELIMINARY PLAT APPROVAL SHALL BE INSTALLED PRIOR TO FINAL PLAT APPROVAL UNLESS A FINANCIAL GUARANTEE HAS BEEN GRANTED FOR THE INSTALLATION OF SAID IMPROVEMENTS.
- 6. PRIOR TO ANY SIGN OR STRIPING INSTALLATION OR REMOVAL, THE CONTRACTOR SHALL CONTACT THE CITY TO ARRANGE FOR AN ON-SITE MEETING TO DISCUSS PLACEMENT AND UNIFORMITY.
- 7. NEW OR REVISED STOP SIGNS, YIELD SIGNS, AND TRAFFIC SIGNALS SHALL BE ADVANCE-WARNED USING THE PROCEDURE OUTLINED IN THE MUTCD. ADVANCE WARNING SIGNS AND FLAGS SHALL BE MAINTAINED BY INSTALLER FOR 30 DAYS AND THEN REMOVED.

SITE PLAN NOTES:

1. ALL RADII IS 5' FROM THE FACE OF CURB UNLESS OTHERWISE NOTED.



PROJECT LAKEWOOD INTERIM LIBRARY
LOCATION 10202 Gravelly Lake Dr SW Lakewood WA 98499
PREPARED FOR PIERCE COUNTY LIBRARY SYSTEM
revision date name 1 8/11/23 ADDENDUM 1 Redline 8/21/23 Addendum 3
PROFESSIONAL STAMP
ABOO INTERURBAN AVE S. SUITE 271 SEATTLE, WASHINGTON 98168 PHONE: (206) 674–4640
SITE PLAN 8/4/2023
SITE BID SET C103 © 2022 BUILDINGWORK, LLC



architecture

preservation

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seattle, washington 98119 office 206 775-8668

www.buildingwork.design

design

20'

40'

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SECTION 015700 - TEMPORARY CONTROLS

PART 1 - GENERAL

1.01 SUMMARY

- A. Section Includes:
 - 1. Provide and maintain controls using methods, equipment, and temporary construction.
 - 2. Protect against unfavorable controls over environmental and other factory and site conditions and related areas under your management. Remove physical evidence of temporary control facilities at completion of Work.
 - 3. Protect adjacent buildings and sitework outside of project area.
 - 4. Coordinate with project phasing.
 - 5. Protect existing utilities to remain both on-site and off-site.
 - 6. Include control provisions for:
 - a. Dust
 - b. Water
 - c. Debris: Disposal management requirements are specified in Section 017419.
 - d. Pollution
 - e. Erosion and sediment
 - f. Protection of work
 - g. Noise
 - h. Fumes (i.e., paints and coatings, exhausts)
 - i. Others, as required
 - 7. Ensure compliance with regulations governing the site and vicinity. Designate one person the Construction Superintendent, or other to enforce provisions preventing:
 - a. Air, water, and soil pollution.
 - b. Waste generation.
 - c. Other irritating, harmful effects.
- B. Related Sections:
 - 1. Section 011100 Summary of Work: Work sequence, Contractor's use of premises
 - 2. Section 015100 Temporary Utilities and Facilities
 - 3. Section 015719 Environmental Controls
 - 4. Section 017129 Cutting and Patching
 - 5. Section 017419 Construction Waste and Disposal Management
 - 6. Section 017423 Final Cleaning

1.02 QUALITY ASSURANCE

- A. Requirements of Regulatory Agencies: See Section 014100 for referenced Codes, ordinances and the like.
 - 1. Where applicable, conform to requirements of state and local air pollution control agency, and other authorities' rules and regulations.
 - 2. Comply with applicable authorities' requirements including those of local utility companies.
- 1.03 DUST CONTROL
 - A. Provide positive methods and apply dust control materials to minimize raising dust from construction operations. Prevent air-borne dust from dispersing into adjacent facilities and the atmosphere.

- B. Block out and/or cover HVAC ducts, enclosures, voids and the like during construction to ensure no dust or fume accumulation.
- 1.04 WATER CONTROL
 - A. Provide methods to control rain water during site erection/installation of prefabricated building until downspouts are permanently connected to stormwater systems. Prevent damage to prefabricated building and adjoining properties.
 - B. Control site installation activities to direct surface drainage away from construction areas, and to direct drainage to proper runoff. Maintain excavations free of water.
 - C. Provide, operate, and maintain hydraulic equipment of adequate capacity to control water.
 - D. Dispose of drainage water in a manner to prevent flooding, and other damage to any portion of the building, site or adjoining properties.

1.05 POLLUTION CONTROL

- A. In accordance with Section 015719, and following:
 - 1. Provide methods, means, and facilities required to prevent contamination of soil, water, or atmosphere. Allow no discharge of noxious substances or fumes from construction operations.
 - 2. Provide equipment and personnel; perform emergency measures required to contain spillages. Remove contaminated soils and liquids.
 - a. Excavate and dispose of earth contaminated by contractor operations off-site in compliance with laws and regulations.
 - b. Replace with suitable compacted fill and topsoil. Provide Owner with receipt of soil acceptability prior to installation.
 - 3. Take special measures to prevent harmful substances from entering public waters.
 - a. Prevent disposal of wastes, effluents, chemicals, or other such substances in or adjacent to bodies of water, or in sanitary or storm sewers.
 - 4. Provide systems for control of atmospheric pollutants in accordance with federal, state, and local published rules and regulations.
 - a. Prevent toxic concentrations of chemicals.
 - b. Prevent harmful dispersal of pollutants into the atmosphere or building HVAC system in the adjacent surrounding buildings.

1.06 EROSION AND SEDIMENT CONTROL

- A. Provide temporary protection of erodible soils during site erection/installation of prefabricated building until downspouts are permanently connected to stormwater systems and installation crews have demobilized from site. Employ methods as may be necessary to effectively prevent erosion and control sedimentation.
- B. Mechanically retard and control runoff rate. This includes construction of diversion ditches, benches, and berms to retard and divert runoff to protected drainage courses.
- C. Temporary erosion and siltation control work shall conform to the local and state requirements except costs for the work shall be considered incidental to and included in the contract.

D. Periodically inspect earthwork to detect any evidence of the start of erosion, apply corrective measures as required to control erosion.

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1.07	STORMWATER POLLUTION PREVENTION PLAN
А.	Contractor is required to create and execute a stormwater pollution prevention plan (SWPPP) that meets the requirements set forth by the City of Lakewood. This plan must be submitted to the AHJ by the contractor prior to the start of work. The City will not issue the final permit until this plan is received.
B.	The SWPP must comply with all elements described in the civil contract documents and include the following:
	 Temporary Erosion and Sedimentation Control (TESC) Inspection log which will be completed by the CESCL and kept on site for review by the City Inpsecor or DOE representative.
	b. A narrative explaining the planned actions for controlling erosion and sedimentation to protect and improve local environmental features
	c. List the ten elements of an effective TESC
	d. A map of the site showing location of each control measure installed. This will be updated as required.
	e. A list of the BMPs you are likely to install.

1.08 PROTECTION OF WORK DURING SITE ERECTION/INSTALLATION/COMPLETION

- A. Provide temporary protection measures for roof seams and other openings in walls or roof during transportation to site, during erection/installation of prefabricated components on site and for all other activities associated with project.
- B. Provide temporary protection for installed products during final completion on site. Control traffic in immediate area to minimize damage.
 - 1. Prohibit traffic or storage upon waterproofed or roofed surfaces.
- 1.09 REMOVAL
 - A. Remove temporary materials, equipment, services, and construction when Architect authorizes.
 - 1. Clean and repair damage caused by installations and use of temporary facilities. Remove temporary control installations. Restore existing facilities used during construction to specified, or to original, condition.

PART 2 - PRODUCTS

Not Used.

PART 3 - EXECUTION

Not Used.

END OF SECTION 015700

<u>1 - GENERAL</u>

- 1.1 SUMMARY
 - A. Furnish labor, material and equipment required for weed removal, placement and amendment of soil for areas to be planted, and the establishment of finish grades as shown on the Drawings and as specified herein.
 - B. Coordinate work with installation of other site work including earthwork, irrigation, seeding, and planting.
 - C. Related sections include the following:
 - 1. Division 01 Section "Temporary Tree and Plant Protection," for protecting trees remaining on-site that are affected by site operations.
 - 2. Division 31 Section "Earth Moving" for preparation of subgrades prior to placement of topsoil and planting soils specified in this section.
 - 3. Division 32 Section "Plants" for planting placement of amended topsoil backfill.

1.2 DEFINITIONS

- A. Finish Grade: Elevation of finished surface of amended topsoil soil.
- B. Manufactured Topsoil: Soil produced off-site by homogeneously blending mineral soils or sand with stabilized organic soil amendments to produce topsoil or planting soil
- C. Amended Topsoil: Native or imported topsoil or surface soil modified with soil amendments and fertilizers.
- D. Noxious Weed or Noxious Weed Seed: Any weed listed in the current edition of the King County Noxious Weed list as a class A, B, or C noxious weed, whether or not control is required
- E. Subgrade: Surface or elevation of subsoil remaining after completing excavation, or top surface of a fill or backfill, before placing planting soil.
- F. Topsoil: See Part 2 Products.
- G. Soil Ripping: Loosening the soil by dragging a ripping shank or chisel thru the soil to the depths and spacing specified, and further defined in this specification.
- H. Soil Tilling: Loosening the surface of the soil to the depths specified with a rotary tine tilling machine, roto tiller, (or spade tiller), and further defined in this specification.

1.3 SUBMITTALS

- A. Product Data: For the following:
 - 1. Fertilizers, including application rates.
 - 2. Soil Amendments.
 - 3. Herbicides.
- B. Samples for Verification: For the following:
 - 1. 1/2 cubic foot compost.
 - 2. 1/2 cubic foot of each imported topsoil. Furnish one sample from each site from which soil is to be furnished.
 - 3. Retain soil and compost submittals on site in sealed, accessible container for comparison to delivered soils.
- C. Product Certificates: For each type of manufactured product, signed by product manufacturer, and complying with the following:
 - 1. Manufacturer's certified analysis for standard products.
 - 2. Analysis of other materials by a recognized laboratory made according to methods established by the Association of Official Analytical Chemists, where applicable.
- D. Qualification Data: For testing agencies.
- E. Material Test Reports: Date of testing on all reports shall be a maximum of 90 days prior to the date of submittal for review.
 - 1. Soil Fertility and Agricultural Suitability Analyses and Recommendations Reports for the following:
 - a. Existing on-site topsoil: From three typical locations as selected by Owner's Representative, minimum 30 days prior to beginning soil preparation work.
 - b. Imported topsoil: Minimum 30 days prior to beginning soil preparation work.
 - c. Amended topsoil: Provide soil analyses and results for soil samples taken from 3 typical locations as selected by Owner's Representative, minimum 7 days after soil preparation work has been completed and prior to installing plants.
 - 2. Compost Analysis: Provide analysis for one representative sample of compost minimum 30 days prior to compost being delivered to Project Site.
 - 3. Compost Maturity: Provide results of Compost Maturity Test when submitting Compost Analysis Report and sample.
 - 4. Soil Compaction Test: Provide results of soil compaction tests minimum of 7 days prior to planting and seeding.
- F. Delivery Slips: Provide delivery slips for each load of delivered material as proof of shipment of specified materials.
- G. Soil Placement Map: Contractor shall provide a plan showing placed location of each load of delivered soil, referenced to delivery slips.

1.4 QUALITY ASSURANCE

- A. Soil Fertility and Agricultural Suitability-Testing Laboratory Qualifications: An independent laboratory, recognized by the State Department of Agriculture, with the experience and capability to conduct the testing indicated and that specializes in types of tests to be performed.
 - 1. Acceptable Soil Testing Laboratories are:
 - a. Western Laboratories, Inc, (800) 658-3858.
- B. Soil Analyses: Furnish soil analyses by a qualified soil-testing laboratory stating:
 - 1. Soil Composition: USDA particle size analysis indicating percentages of sand, silt and clay, and percent organic matter.
 - 2. Macro and micro nutrient fertility tests as determined by pH, salinity, nitrate nitrogen, ammonium nitrogen, phosphate phosphorous potassium, calcium, magnesium, soluble copper, zinc, manganese, iron, saturation extract boron and sodium analyses.
 - 3. Sodium Absorption Ratio (SAR).
 - 4. A Cover Letter shall be provided summarizing existing soil conditions and the Laboratory's recommendations.
 - 5. Recommendations by the soil testing lab for fertilizer and soil amendments in pounds per 1,000 square foot or tons per acre, as necessary to correct soil deficiencies.
 - 6. Noxious Weed Germination Test: a minimum of one 36 inch square by 3 inch deep soil sample for each topsoil source considered for use on the project. Place soil in tray with adequate drainage layer beneath, keep soil moist (not saturated) for 7 days in a temperature controlled greenhouse environment, provide photos and written report summarizing germination results.
- C. Compost Testing Laboratory Qualifications: An independent laboratory, with the experience and capability to conduct the testing indicated following U.S. Composting Council Seal of Testing Assurance (STA) procedures, or equivalent.
- D. Compost Analysis: Provide documentation from supplier that compost has reached a monitored temperature of 140 degrees Fahrenheit for at least one week. Engage an independent soil testing laboratory to test representative sample(s) of compost and furnish compost analysis report for the following parameters:
 - 1. Percent organic matter, percent moisture, percent inerts (foreign matter), pH, soluble salts, and particle size.
 - 2. Nutrient content, including: Nitrogen (N), Phosphorus (P), Potassium (K), Calcium (Ca), and Magnesium (Mg) and Sulfur (S).

- 3. Trace Metals, including: Arsenic (As), Cadmium (Cd), Chromium (Cr), Copper (Cu), Lead (Pb), Mercury (Hg), Nickel (Ni), and Zinc (Zn).
- 4. Maturity Indicator. Provide bio-assay results. Provide Carbon-Nitrogen ratio.
- 5. Stability Indicator: Provide respiration test results.
- E. Request inspection and allow observation by Owner's Representative of prepared soils before planting.
- F. Soil Compaction Testing: Furnish soil compaction standard tests per ASTM 698. Request inspection and allow observation by Owner's Representative of prepared soils before planting.

1.5 DELIVERY, STORAGE AND HANDLING

- A. Deliver packaged materials in manufacturer's unopened containers fully identified by name, brand, type, weight and analysis.
- B. Store and handle packaged materials to prevent damage and intrusion of foreign matter.
- C. Store stockpiled topsoil in area designated by Owner's Representative. Provide erosion control measures for stockpiled topsoil on site to prevent contamination of the soil. Refer to Division 31 Section "Earth Moving" for control of dust and erosion.

1.6 SOIL AMENDMENT BID QUANTITIES

- A. Bid quantities and types of soil amendments shall be based upon those listed in this Section. Types of amendments required and quantities shall be adjusted as necessary based upon actual results of soil fertility and agricultural suitability analyses and recommendations for on-site topsoils.
- B. Amount per 6-inch lift of topsoil over 1000 square-feet of landscape area:
 - 1. 25 lbs. Gypsum (Calcium sulfate)
 - 2. 35 lbs. Calcium carbonate limestone 'Calpril'
 - 3. 35 lbs. Dolomite limestone 'Dolpril'
 - 4. 8 lbs. Treble superphosphate (0-45-0)
 - 5. 3 lbs. Ammonium nitrate
 - 6. 4 ozs. Zinc sulfate
 - 7. 8 ozs. Manganese sulfate
 - 8. 1 oz. Laundry Borax
 - 9. 6 cu-yds Compost

1.7 SITE CONDITIONS

A. Topsoil placement and soil preparation shall not take place during periods where saturated soil or surface water is present in work areas.

B. Work shall not take place when temperature is less than 32 degrees Fahrenheit, or when frozen soil exists on site.

1.8 COORDINATION

- A. Coordinate soil preparation with Division 31 Section "Earth Moving" such that topsoil, soil amendments and fertilizers are incorporated into ground fill areas in specified lifts and to specified depths below finish grade for planting and lawn areas. Topsoils shall be amended per recommendations of the Soils Testing Laboratory.
- B. Coordinate soil preparation with timing and procedures for installation of related site work including irrigation, seeding, and planting.

PART 2 - PRODUCTS

- 2.1 TOPSOIL
 - A. Topsoil Definition: ASTM D 5268; natural or cultivated surface-soil layer containing organic matter and sand, silt, and clay particles, conforming to USDA classification for Loam or Sandy Loam; friable, pervious, and black or a darker shade of brown, gray, or red than underlying subsoil; reasonably free of subsoil, clay lumps, gravel, and other objects more than 1 inches in any dimension; and free of weeds, roots, and other deleterious materials, with the following physical properties:
 - 1. Organic Matter: 6 percent minimum to 10 percent maximum.
 - 2. Sodium Adsorption Ratio (SAR): less than 6.0.
 - 3. Saturation Extract concentration for Boron: less than 1.0
 - 4. pH range of from 6.5 to 7.5 (Saturation Extract Conductivity: less than 4.0 dS/m @ 25 degrees Celsius as determined in a saturation extract.
 - 5. Non-soil components: less than 1 percent by volume.
 - 6. Heavy metal concentrations: below the USDA per year load limit.
 - 7. Minimal weed seed.
 - a. If regenerative noxious weeds are present in the soil, all resultant growth including roots shall be removed throughout one-year period after acceptance of work at no additional cost to Owner.
 - B. Topsoil Source: Reuse surface soil stockpiled on-site. Verify suitability of stockpiled surface soil to produce topsoil. Clean surface soil of roots, plants, sod, stones, clay lumps, and other extraneous materials harmful to plant growth. Ensure no contamination of the soils occurs during earthwork and grading, and that the soil remains friable and free of debris.
 - 1. Import Topsoil: Supplement on-site topsoil with imported or manufactured topsoil from off-site sources when quantities are insufficient. Import topsoil is subject to approval and shall conform to USDA soil texture class "Loam" certification by Soil Testing Analysis, no more than 12 months prior to delivery to the site. Obtain

topsoil displaced from naturally well-drained construction or mining sites where topsoil occurs at least 4 inches deep; do not obtain from agricultural land, bogs or marshes.

a. Provide one of the following as Import Topsoil:

- 1) Cedar Grove, 3-Way Topsoil, (877) 764-5748
- 2) Pacific Topsoils, Inc., 3-Way Topsoil, (425) 337-2700

2.2 INORGANIC SOIL AMENDMENTS

- A. Dolomitic Lime: Natural, agricultural limestone (calcium and magnesium carbonate) containing a minimum of 20 percent calcium and 11 percent magnesium and as follows:
 - 1. Screen Analysis: 100 percent passing through No.30 sieve; 70 percent passing through No. 100 sieve; and minimum 30 percent passing through No.325 sieve.
 - 2. Provide lime in form of granulated, prilled, dolomitic limestone, 'DoloPril' by Pacific Calcium, Inc., (877) 571-3555, or equal.
- B. Calcitic Lime: Natural, agricultural limestone (calcium carbonate) containing a minimum of 36 percent calcium and as follows:
 - 1. Screen Analysis: minimum of 100 percent passing through No. 10 sieve and a minimum of 80 percent passing through No. 100 sieve.
 - 2. Provide lime in form of granulated, prilled, limestone, 'CalPril' by Pacific Calcium, Inc., (877) 571-3555, or equal.
- C. Sulfur: Granular, biodegradable, containing a minimum of 90 percent sulfur, with a minimum of 99 percent passing through No. 6 sieve and a maximum of 10 percent passing through No. 40 sieve.
- D. Iron Sulfate: Granulated ferrous sulfate containing a minimum of 20 percent iron and 10 percent sulfur.
- E. Aluminum Sulfate: Commercial grade, unadulterated.
- F. Gypsum: Agricultural gypsum; minimum 90 percent calcium sulfate, finely ground with 90 percent passing through No. 50 sieve.
- G. Sand: Clean washed river sand, free of calcium, chlorides and other deleterious substances.

2.3 ORGANIC SOIL AMENDMENTS

- A. Compost: Well-decomposed, commercially manufactured, stable, and weed-free organic matter, no food waste shall be a part of the compost. pH range of 5.5 to 7.5; 100 percent passing through 1/2-inch sieve; soluble salt content of 2.5 to 7.5 decisiemens/m; not exceeding 0.5 percent inert contaminants and free of substances toxic to plantings; and shall conform as follows:
 - 1. Tested, at minimum, every six months for noxious weeds.

- 2. Organic matter source (feedstock): Agricultural, food, or industrial residuals; biosolids; yard trimmings; or source-separated or compostable mixed solid waste.
- 3. Organic Matter Content: 50 to 70 percent of dry weight as determined by ash method.
- 4. Moisture Content: 40 to 55 percent by weight
- 5. Free of refuse (less than 1 percent by dry weight), plastics, contaminants or any material toxic to plant growth.
- 6. Processed to meet U.S. Composting Council's Seal of Testing Assurance (STA) Program, or equivalent.
- 7. Carbon to Nitrogen Ratio: 30 to 1 or lower.
- 8. Composted for a minimum of 120 days and reach a monitored temperature of 140 degrees Fahrenheit for at least one week.
- 9. Available Products and Suppliers:
 - a. Cedar Grove Composting., Compost , phone (877) 764-5748.
 - b. Pacific Topsoils, Inc., Compost, phone (425) 337-2700
 - c. Or approved equal.

2.4 FERTILIZER

- A. Fertilizer composition and rate to be determined based upon soil analysis. For bidding purposes, assume: 10 Nitrogen (N), 10 Phosphorus (P), 10 Potassium (K), 5 Sulfur (S) applied at a rate of 10 pounds per 1000 square feet in all planting beds and seeded areas.
- B. Bonemeal: Commercial, raw or steamed, finely ground; a minimum of 4 percent nitrogen and [10] [20 percent phosphoric acid.
- C. Superphosphate: Commercial, phosphate mixture, soluble; a minimum of 20 percent available phosphoric acid.
- D. Commercial Fertilizer: Commercial-grade complete fertilizer of neutral character, consisting of fast- and slow-release nitrogen, 50 percent of urea formaldehyde, phosphorous, and potassium in the following composition:
 - 1. Composition: Nitrogen, phosphorous, and potassium in amounts recommended in soil reports from a qualified soil-testing agency.
- E. Slow-Release Fertilizer: Granular or pelleted fertilizer consisting of 50 percent waterinsoluble nitrogen, phosphorus, and potassium derived from natural organic and inorganic sources in the following composition:
 - 1. Composition: Nitrogen, phosphorous, and potassium in amounts recommended in soil reports from a qualified soil-testing agency.

2.5 MISCELLANEOUS PRODUCTS

- A. Post-Emergent Herbicide: Select one of the following: "Glyphogan Plus" by Mana, "Envoy Plus" by Valent, "Crossbow" by Dow AgroSciences, "Landmaster BW" by Agri Star or approved equal.
- B. Pre-Emergent Herbicide: "Ronstar-G" by Bayer, "Dimension EC," by Dow AgroSciences or equal. Products containing either pendimethalin or DCPA are prohibited.
- C. Contact Herbicide for controlling nutsedges: "SedgeHammer" by Gowan.

PART 3 - EXECUTION

3.1 EXAMINATION OF SITE CONDITIONS

- A. Examine for site conditions that will adversely affect execution, permanence, quality of work, and survival of plant material and grasses.
- B. Identify areas to receive planting and lawn on site.
- C. Verify that subgrades and slopes of lawn and planting areas are acceptable to Owner's Representative prior to commencing work of this Section.
- D. Should the Contractor find any discrepancies between the Drawings and the physical conditions, inform the Owner's Representative immediately for clarification.
- E. Begin Work required under this Section only after conditions are satisfactory.

3.2 PREPARATION

- A. Protect structures, utilities, sidewalks, pavements, and other facilities, and existing lawns and exterior plants from damage caused by soil preparation operations.
- B. Prepare soils at a time when moisture conditions will permit proper cultivation.
- C. Remove stones over 1-inch diameter, sticks, roots, mortar, concrete, rubbish, debris, and all materials harmful to plant life, and legally dispose of them off Owner's property.
- D. Remove or spray as required to eradicate noxious weed growth and roots.
 - 1. Achieve complete removal or kill of all weeds within all areas receiving new plantings and lawn areas.
 - 2. In planting beds, kill achieved by working soil is permissible for annual non-noxious broad-leaf type weeds.
 - 3. Apply post-emergent herbicide over all areas of weed or grass growth within landscaped area to eradicate weed growth and roots. Apply in two applications at manufacturer's maximum recommended rate, as follows:
 - a. First application: Apply 7 days prior to performing soil preparation.

- b. Second application (to kill new vegetation): Apply after soil preparation has been completed and minimum of 48 hours prior to planting.
- c. Observe manufacturer's recommended period prior to working in treated areas.
- 4. Apply contact herbicide directly onto foliage of nutsedges. In areas of established lawn grasses infested with nutsedge, apply herbicide by wicking. Do not spray.
- E. Locate and securely mark or flag irrigation sprinkler heads, area drains, catch basins, clean outs, manholes, valve boxes, and other site improvements not extending above finish grade.
- F. Provide erosion-control measures to prevent erosion or displacement of soils and discharge of soil-bearing water runoff or airborne dust to adjacent properties and walkways, in accordance with Division 31

3.3 SOIL PREPARATION FOR PLANTING AREAS

- A. This article pertains to planting areas as shown on the Drawings where mass plantings of trees, shrubs and ground cover plants are scheduled.
- B. Excavate 24 inch deep by 12 inch wide pits for percolation testing where planting areas occur in soils compacted due to construction traffic, materials staging, stockpiles exceeding 72 inch height and areas of soil surcharging. Prepare a minimum of ten (10) test pits in locations selected by the Owner's Representative representing the full range of planting areas on site.
 - 1. Fill holes to the top with water and let stand for 1 hour minimum.
 - 2. Refill hole to top with water and measure total depth.
 - 3. Allow hole to drain for 2 to 3 hours and measure total depth of water.
 - 4. If soil drains at a rate of less than 2 inches per hour prepare subgrades in accordance with procedures for poor draining soils.

 Prepare subgrades as per detail 4 on sheet L102 in the bid drawing set. In areas of poor draining soils prepare subgrades by excavating and removing soil, rock and other construction material to 24 inches minimum below finish grade. Cross-rip subgrades to depth of 6 inches prior to placing topsoil. Retest percolation and modify subgrade until 2 inches per hour percolation is obtained. Adjust quantity and depth of placed topsoil as necessary to achieve finished grade as shown on plans. See Division 31 Section "Earth Moving" for excavation and preparation of subgrades. 	C.	Plar	nting area subgrade preparation:
		1. 2.	In areas of poor draining soils prepare subgrades by excavating and removing soil, rock and other construction material to 24 inches minimum below finish grade. Cross-rip subgrades to depth of 6 inches prior to placing topsoil. Retest percolation and modify subgrade until 2 inches per hour percolation is obtained. Adjust quantity and depth of placed topsoil as necessary to achieve finished grade as shown on
		3.	I

- D. Planting beds and seeded areas: Place 8 inches of topsoil, compost, soil amendments, and fertilizers as recommended in Agricultural Soil Suitability Report per 1,000 square feet and rototill thoroughly to a depth of 4 inches. Compost shall constitute 5% of the amended soil. Place remainder of topsoil, compost, soil amendments, and/or fertilizers as recommended in Agricultural Soil Suitability Report per 1,000 square feet and rototill thoroughly to a depth of 8 inches, allowing for compaction, natural settlement, and depth of specified mulch.
- E. Concrete Planters: Place 8 inches of topsoil, compost, soil amendments, and fertilizers as recommended in Agricultural Soil Suitability Report per 1,000 square feet and rototill thoroughly to a depth of 4 inches. Compost shall constitute 5% of the amended soil. Place the remainder 4 inches of topsoil, compost, soil amendments, and fertilizers as

recommended in Agricultural Soil Suitability Report per 1,000 square feet and rototill thoroughly to a depth of 4 inches, allowing for compaction, natural settlement, and depth of specified mulch.

- 1. It is the Contractor's option to set up a facility on-site for the preparation and amendment of topsoils, instead of preparing and amending the topsoils in place as indicated in the paragraph above.
- 2. Set up facility in location as directed by Owner's Representative.
- F. Water lightly and allow planting mix to settle. Add additional material at mixture indicated in paragraph above to bring soil level to grades shown on the Drawings with allowance at pavement edges for mulch placement. Provide compaction to 80 percent maximum relative density or as indicated in Division 31 Section "Earth Moving."
- G. Meet lines, grades and elevations shown, after light rolling and natural settlement. Fine grade shrub and ground cover areas to smooth even surface with loose, uniformly fine texture. Rake and drag shrub and ground cover areas to remove ridges and fill depressions to obtain firmness and finish grades preparatory to receiving planting.
- H. Remove stones over 1/2-inch in any dimension and sticks, roots, rubbish and other extraneous matter.

3.4 SOIL PREPARATION FOR PLANTING PITS OF TREES

- A. This article pertains to tree planting when occurring on an individual basis.
 - 1. Backfill Mix: Prepare backfill mix and place in planting pits as specified in Division 32 Section "Plants."
 - 2. Grade smooth to elevations shown.

3.5 SOIL PREPARATION UNDER EXISTING TREES

- A. Remove vegetation not indicated to remain beneath canopy of existing trees. Take care not to disturb roots of existing trees.
- B. Lightly rake areas and add amended topsoil to meet proposed grades.

3.6 FINE GRADING

- A. Finish grade after full settlement including mulch, shall be 1 inch below tops of curbs, walks, or existing grades in shrub areas and 3/4 inch lower in lawn areas.
- B. Slope all areas to prevent puddling and drain surface water toward catch basins, drains, curbs, or off-site as shown on Drawings.
- C. Soil in all areas shall be thoroughly settled, with a smooth surface free of humps and hollows, and shall be firm enough to resist undesirable impressions when stepped upon.
- D. Use levels, screens, drags, or any other equipment necessary to establish and verify grades and surfaces.
- E. Finish grade lawn, grass and planting areas to smooth, even surface with loose, uniformly fine texture.

- F. Notify Owner's Representative 36 hours in advance to review fine grading of lawn, grass and planting areas. Finish grades shall be prepared to the satisfaction of the Owner's Representative prior to planting.
- G. See Division 32 Section "Plants," for mulch placement.

3.7 CLEAN-UP

- A. Clean up excess materials and debris from project site upon completion of work or sooner if directed by the Owner's Representative.
- B. Leave in neat and tidy condition daily.

3.8 DISPOSAL

A. Disposal: Remove surplus soil and waste material, including excess subsoil, unsuitable soil, trash, and debris, and legally dispose of them off Owner's property.

END OF SECTION

FINAL Geotechnical Report

Lakewood Interim Library

Lakewood, Washington

April 2023



Contact Steven Halcomb, PE, GE, DGE shalcomb@crweng.com

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Final Geotechnical Report Lakewood Interim Library Lakewood, Washington

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April 2023 CRW Project Number 52501.00

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Figure

Figure 1 – Site Overview and Borehole Locations

Appendices

Appendix A – Borehole Logs Appendix B – Laboratory Results

1. Introduction and Project Description

CRW Engineering Group, Inc. (CRW) is pleased to present this geotechnical data and design recommendations report to support the development of a new interim library located at 10202 Gravelly Lake Drive SW in Lakewood, Washington. The project includes a modular library building, a new parking lot, sidewalks, light poles, water and sewer service utilities, and landscaping. A geotechnical investigation was conducted by CRW for BuildingWork.

The scope of work included:

- Reviewing historical soil investigations within and near the project area;
- Performing a geotechnical investigation which included soil borings placed based on expected development of the site;
- Installing a piezometer for groundwater level monitoring;
- Overseeing laboratory testing of recovered soil samples including moisture content and gradation;
- Analyzing field observations and testing results; and,
- Preparing the geotechnical report to provide recommendations.

2. Site Conditions

The project is located at 10202 Gravelly Lake Drive SW in Lakewood, Washington, on the corner lot west of Gravelly Lake Drive SW and south of Alfaretta Street SW (Figure 1). The site is flat and is currently undeveloped, maintained as a mowed field with small ornamental trees at the northern edge of the lot. Concrete sidewalks border the site on the north and east boundaries. A vacant lot of similar size borders the site to the west, and a small commercial building with paved parking lots borders the site to the south. The property and the adjacent lot to the west are surrounded by a temporary chain-link fence approximately 6 feet tall. The fence separating the two lots has fallen to the ground.

Environmental reports indicate that this site was developed as a service station in the 1920s and used for this purpose until the early 2000s. All above-grade infrastructure formerly on this site has been removed and buried fuel storage tanks and piping were documented as having been removed in April 1992. Remediation of the site was achieved through removal of contaminated soil. After remediation, the site was backfilled with clean fill reported to be pea gravel and native soil. The site was restored to a level grade (Pacific Environmental, 1992).

2.1 Geology

The surficial geology in the Lakewood area was determined from the Geologic Map of the City of Tacoma, as published by M. Smith (1977) in addition to more recent digital versions of Washington geological maps available on the Washington State Department of Natural Resources website. Soils in the Lakewood area are described as part of the Vashon Drift, Pleistocene-age glacially-derived mineral soils. Sub-groups of the Vashon Drift include outwash and till deposits. Loosely-compacted recessional outwash deposits of sand and gravel are generally found above dense till deposits. Till deposits are described as a dense, poorly-sorted, and non-stratified mixture of gray to blue clay, silt, sand, gravel, and cobbles with occasional large boulders. Clasts are subangular to rounded.

Original site fill beneath formerly asphalt-paved surfaces was described as "damp clayey gravel," while native soil described as sandy gravel and cobbles was observed to a depth of 16 feet below ground surface (BGS) (Pacific Environmental, 1992). A later investigation noted predominantly dense silty sand or silty gravel with 5 to 20 percent cobbles by volume and up to 20 percent fines to a depth of 31 feet BGS. Clean sand and poorly-graded gravel were also noted in some holes (Delta Environmental, 2001).

2.2 Historical Soils Investigations

Historical geotechnical data was not provided to CRW. Environmental investigations included boring logs describing soil conditions on some parts of the site, but with limited geotechnical information.

2.3 Contaminated Sites

The State of Washington Department of Ecology (DOE) Toxics Cleanup database was reviewed for information about the contaminated site identified at the project site. This site is listed with a status of "Cleanup Complete - No Further Action." Cleanup Site ID (CSID) is 7082.

3. Field Investigation

A geotechnical investigation was performed on 12 and 13 January 2023 to assess existing soil conditions. The investigation drilled and sampled four boreholes (BH-01 through BH-04) located in areas indicated as being proposed parking lot or building locations, see Figure 1.

3.1 Subsurface Drilling

Holt Services, Inc. of Edgewood, Washington provided drilling services, using a truck mounted Mobile Drill B-60 rig equipped with a nominal 8-inch outer diameter (O.D.) hollow-stem auger to advance the boring. Utilities were located prior to drilling by submitting a locate request to 811.

A CRW engineer supervised the field investigation, managed field operations, and logged the recovered soil samples. Borings were advanced to various depths from 16.5 to 30.92 feet BGS (depth of the last split-spoon advanced beyond the auger). Borehole logs are presented in Appendix A.

3.2 Sample Collection

Soil samples were obtained by advancing a standard split-spoon sampler into the soil beyond the bottom of the auger. Driven samples were collected using a 2-inch O.D. split-spoon sampler via the Standard Penetration Test (SPT). The sampler was advanced 18 inches, counted in 6-inch intervals, using a 140-pound auto-hammer. The number of blows required to drive the sampler each 6-inch interval is reported on the borehole logs. The blow counts shown on the borehole logs are field values that have not been corrected for overburden, sampler size, hammer energy, rod length, or other factors.

Split-spoon samples were collected at approximately 2.5-foot to 5-foot intervals depending on observed lithology. Recovered samples were visually classified in the field before being individually sealed in double plastic bags and transported to Alaska Testlab (ATL) in Anchorage, Alaska for additional testing. Field visual classifications were verified with laboratory testing on selected samples. Soil characteristics, such as classification, consistency, moisture, and color were noted for each sample recovered. Classification was performed following the Unified Soils Classification System (USCS) according to ASTM D2487/D2488.

3.3 Borehole Completion and Monitoring Well Installation

One borehole (BH-01) was completed as a monitoring well for groundwater level monitoring. The unique well ID for this monitoring well is BPW 491. A schedule 40 2-inch nominal diameter polyvinyl chloride (PVC) pipe with threaded connections was installed over the length of the boring, with machine-slotted 0.020-inch screen from 15.5 to 30.5 feet BGS. The annular space was filled with graded 2x12 silica sand from 13 to 30.5 feet BGS. Above 13 feet BGS, hydrated bentonite chips were used to seal the annular space to a depth of 2 feet BGS. The well casing was fitted with a locking plug and finished with a steel flushmount monument installed level with the surrounding ground surface and set in concrete to a depth of 2 feet BGS. A well construction diagram will be prepared by Holt Services and submitted to the WA DOE as required.

Boreholes not completed as monitoring wells were backfilled with soil cuttings.

3.4 Groundwater Monitoring

Groundwater levels were noted during and immediately after drilling. Additional groundwater level measurements were collected after completion of drilling as summarized later in this report.

3.5 PID Field Screening

No field screening was performed. No visual or olfactory evidence of contamination was observed during the investigation.

Soil laboratory tests to evaluate index properties of representative samples were performed by the Alaska Testlab (ATL) in their Anchorage, Alaska facility. The laboratory testing program consisted of soil index tests to determine the water content, grain-size distribution, and limited mechanical analysis (LMA). LMA consists of washing a sample over the Number 200 mesh sieve. The coarse fraction of the remaining soil is then dried and sieved through the Number 4 sieve to determine the sand and gravel content. The LMA is a means to determine the percentage of coarse and fine soil in a sample without having to perform full gradations. The laboratory tests were performed in accordance with the test methods of ASTM International or ATL's in-house procedure as listed in Table 4-1.

Analysis	Method	Number of Samples
Water Content	ASTM D2216	31
Grain-size Distribution	ASTM D6913 ASTM D422	4
Limited Mechanical Analysis	ASTM D1140 In-house procedure	11

Results of the laboratory testing are presented in Appendix B.

5. Investigation Findings

5.1 Soil Lithology

Soil in the upper five feet BGS were observed to be poorly or well-graded gravel with sand, except BH-01 where laboratory analysis indicated that the fines content was five percent. In BH-01, most of the lithology to 20 feet BGS is imported fill, based on what is known about the history and past use of the site, with native soils present beyond this depth. In BH-02, the upper five feet BGS is likely imported fill with native soils at depth. In BH-03 and BH-04, drilling action indicated that native soils may start at two to three feet BGS.

Native soils are poorly to well graded gravels and sands with variable fines content containing cobbles up to eight inches in diameter. In a few locations, silty sand or silty gravel were observed.

Fines content in native soils generally ranges from three to ten percent in gravelly and cobbly soils, while in siltier intervals it was measured up to 26 percent. Particle shape was generally subrounded to rounded, with some angular sand and subangular gravel.

5.2 Contaminated Soils

No evidence of petroleum-contaminated soils was observed during this investigation. No odor or sheen was observed. No field screening was performed.

5.3 Groundwater Conditions

Groundwater was observed at approximately 20 feet BGS in BH-01 and BH-02. BH-03 and BH-04 were not advanced past 16.5 feet BGS, and no groundwater was observed in these boreholes. Groundwater level readings were collected in BH-01 on 12 and 13 January 2023. Groundwater levels observed during and after drilling are presented on the borehole logs and in Table 5-1 below.

Devehale	Depth to Water (feet BGS)		Piezometer		
Borehole Designation	At Time of Drilling	Immediately After Drilling	23 Hours After Drilling	Screened Interval (feet BGS)	PVC Total Depth (feet BGS)
BH-01	20	19.7	18.8	15.5 – 30.5	30.5
BH-02	20	-	-	-	-
BH-03	Not Observed	-	-	-	-
BH-04	Not Observed	-	-	-	-

Table 5-1. Groundwater Levels

5.4 Seismic Considerations

The project site lies in a region of moderate to high seismicity and may be subjected to relatively large earthquakes and strong ground motion.

Design parameters were determined from the American Society of Civil Engineers' (ASCE) online hazards tool (<u>https://asce7hazardtool.online/</u>) and the United States Geological Survey (USGS) online Unified Hazard Tool (<u>https://earthquake.usgs.gov/hazards/interactive/</u>). Table 5-2 provides general seismic design parameters for the 2,475-year return period consistent with Section 1613 of the International Building Code (International Code Council, 2021) with any applicable State of Washington and City of Lakewood amendments and Chapter 11 of ASCE 7-16 (2016) assuming risk category II. Based on our borings, experience, and judgment, we estimate the site to be designated as Site Class D though due to

the requirements of ASCE 7 (discussed below), only the peak ground acceleration (PGA) is adjusted for site class. Other spectral acceleration values are for bedrock ground motions.

Description	Values
Moment Magnitude, M _w (Mean/Largest Mode)	7.4/7.1
PGA _M (adjusted for site class)	PGA _M =0.55g
MCE_R ground motion (period = 0.2s) – Bedrock motion	S _S = 1.35g
MCE _R ground motion (period = 1.0s) – Bedrock motion	S ₁ = 0.471g

We note that, unless the exceptions apply, ASCE 7-16 requires either a site response analysis (SRA) or ground motion hazard analysis (GMHA) be performed to obtain the site's full design response spectrum. SRA or GMHA are beyond the scope of this geotechnical report. We recommend the structural engineer review the exceptions in ASCE 7-16 to evaluate whether the full design response spectrum is required. CRW's geotechnical engineers will aid with further efforts as the design progresses.

6. Geotechnical Engineering Recommendations

Based on our findings and results of our laboratory testing, we have developed the following recommendations based on our understanding of the project.

6.1 Frost Depth

Seasonal frost was not observed at the time of drilling. We understand the IBC with City of Lakewood local amendments specifies a design frost depth of 12 inches.

6.2 Stability Evaluation

6.2.1 Slope Instability

The site is relatively flat, therefore, by inspection, global instability is deemed of no concern.

6.2.2 Loss of Bearing Capacity

Assuming the foundations do not bear on deleterious material, an inspection of blow counts and soil type suggest that the risk of loss of bearing capacity during a seismic event is moderate. Due to the presence of unsaturated liquefiable soils (see below), we recommend a reduced seismic bearing capacity as discussed later in this report.

6.2.3 Liquefaction and Lateral Spreading

Liquefaction is the result of the buildup of excess pore water pressure, beyond hydrostatic, generated in an undrained soil loading condition induced by seismic shaking. In this condition, partial or complete loss of inter-particle friction within the soil mass occurs, resulting in dramatic decrease of the soil's shear strength (Kramer, 1996; Idriss and Boulanger, 2008).

We screened the site for potential liquefaction based on grain size distribution, depth of water, and blow counts. We noted the site was predominantly gravel which resists liquefaction and makes typical liquefaction assessments difficult. Based on inspection of the blow counts, we consider liquefaction potential across most of the site to be low to negligible.

In BH-01, we noted low blow counts in unsaturated gravels from approximately 5 to 20 feet BGS, likely due to poor compaction of the fill. While not saturated, conditions could lead to post-earthquake settlements even in unsaturated sands and gravels, therefore we performed a preliminary liquefaction analysis for dry sands following Pradel (1998). We note that Pradel's work is for sands whereas this site is predominantly gravel therefore we believe our results are conservative though we do not know by how much. The results of our preliminary analysis determined total post-earthquake settlements on the order of 1.2 inches in BH-01. Settlements from the other boreholes are expected to be near zero based on the blow counts. The exact extent of the poorly compacted existing fill is unknown. We estimate, based on historical imagery and where the extent of the previous excavation occurred, the differential settlement to be on the order of 1.2 inches over 18 feet.

Liquefaction-induced lateral deformations are termed lateral spreading. Lateral spreading was evaluated considering the method outlined by Youd et al. (2002). The procedure considers the earthquake magnitude, distance to the seismic source, thickness of the liquefiable layer, fines content, average particle size, and slope of the terrain. The average lateral spreading is estimated to be less than 0.5 inches of movement.

6.3 Shallow Foundations

6.3.1 Bearing Capacity, Settlement, and Lateral Loading

The existing conditions are conductive to shallow foundations in the form of spread or continuous footings. We presume for this report conventional footing depth will be utilized assuming the differential settlement due to seismic-induced post-liquefaction settlements can be accommodated by the structure. If the differential settlement cannot be accommodated by the structure, we recommend relocating the building, overexcavating and replacing poorly compacted existing fill around BH-01 (discussed later), or performing ground improvement (discussed later). In addition, we are aware that sometimes frost protected shallow foundations (FPSF) are considered. Recommendations for FPSF can be provided on request.

The design of shallow foundations must consider the bearing capacity of the underlying soil in addition to the potential for settlement, effects of seasonal frost, susceptibility to erosion/expansion, and loss of bearing due to seismic events. In general, designed foundations should be consistent with current standard of practice and appropriate building code(s). Table 6-1 summarizes recommended bearing capacity and settlement values for shallow foundations. We recommend shallow foundations bear directly on the native granular material, provided that the underlying soils are consistent with conditions observed in the attached borehole logs.

Description	Value
Allowable bearing pressure (psf) ¹	Static conditions – 3,000 Seismic conditions – 1,500
Minimum/Maximum width (feet)	2/8
Minimum exterior footing embedment below finished grade (feet) –warm footing	2.5
Minimum interior footing embedment below finished grade for warm foundations (inches)	12
Approximate total settlement (inches) ³	1.0
Estimated differential settlement (inches) ³	0.5

Table 6-1. Shallow Foundation Bearing Values

1. Includes a factor of safety 2.5

2. pcf – pounds per cubic foot, psi/in – pounds per square inch per inch, psf – pounds per square foot

3. Excludes post-liquefaction settlement

These recommendations apply to footings prepared in accordance with our recommendations, isolated from adjacent footings, not eccentrically loaded, and not on a slope. If the footings are not prepared in accordance with our recommendations or other conditions prevail, the bearing capacity values will require reduction.

6.3.2 Uplift

Uplift loads may occur in some foundation elements due to overturning moments resulting from wind and seismic forces. Uplift loads may be resisted by the weight of the footing and soil within the limits of a truncated pyramid above the top of the footing. The shape of the truncated pyramid will vary with material type and density. For the expected fill, the pyramid should be defined by a 16-degree angle α , as shown in Exhibit 6-1, measured from a vertical line extending upward and away from the top edge of the footing.

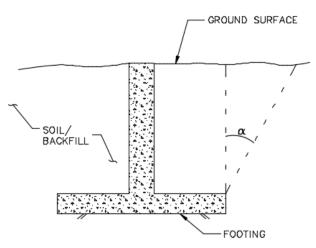


Exhibit 6-1 – Uplift Resistance

6.3.3 Slab Foundation

Slabs-on-grade may be used outside of mat foundations (if constructed). Conventional slabs may be supported on-grade, provided the subgrade soils are prepared as recommended in Section 7.3. We recommend that the slab be founded on either undisturbed native soils or on engineered fill placed over the undisturbed native soils. For any slab foundations, we recommend the use of a subgrade reaction modulus for design. The modulus of subgrade reaction is not an intrinsic property of the soil, but depends on the dimension and the stiffness of the slab. Assuming our recommendations are followed, a coefficient of subgrade reaction, K1, for a 1-foot diameter plate of 250 pounds per cubic inch (pci) can be used for design. This value can be adjusted for use as the subgrade reaction for the mat foundation per the designer's procedure.

We recommend the mat foundation be designed to tolerate a 1-foot cantilever and 2-foot internal span.

We recommend that the slab-on-grade floors be underlain by a 6-inch-thick capillary break consisting of material meeting the requirements of Mineral Aggregate Type 22 (¾-inch crushed gravel), City of Seattle Standard Specifications for Road, Bridge, and Municipal Construction (2020 Edition) 9-03.16, or approved equal.

Provided that loose soil is removed and the subgrade is prepared as recommended, we estimate that slabs-on-grade will not settle appreciably. If loose soils are not completely removed and replaced with properly compacted fill, the potential settlement may be mitigated using bi-axial geogrid beneath the building foundation. The use of geogrid will not completely eliminate the potential for movement but will minimize differential settlement. We recommend the geogrid to be installed around BH-01 to the limits of the historic excavation in that location. CRW's geotechnical will work closely with the civil and structural engineer to provide input for the limits of the geogrid. We anticipate the geogrid to be installed in the northeastern portion of the building footprint, based on the current layout, and extending no more than 8 feet beyond the outer edge of the building foundation where required.

The geogrid should be consistent with Table 3 of Section 9-33.2(1) of the Washington State Department of Transportation (WSDOT) Standard Specifications for Road, Bridge, and Municipal Construction M 41-10, 2023 Edition with similar mechanical properties to Mirafi BXG11. We recommend a minimum of two layers of geogrid with the bottom layer installed between existing subgrade and classified fill and the second layer a minimum of 1 foot above the bottom layer. The geogrid should be installed per the manufacturer's recommended procedures and practices.

An underslab drainage system to remove water from below slabs-on-grade is not considered necessary for this site.

6.4 Pavement Sections

We understand that paved parking lots handling light traffic (predominantly passenger cars and pickups) are to be constructed. The following pavement recommendations were developed based on the Federal Highway Administration's NHI-05-037, Geotechnical Aspects of Pavements (2006), the American Association of State Highway and Transportation Officials (AASHTO) Guide for Design of Pavement Structures (1993), and the City of Lakewood Engineering Standards Manual (2021). We recommend pavement structural sections presented in Tables 6-2 and 6-3 for the parking lot and sidewalk. Material specifications can be found in Section 9-03 of the WSDOT Standard Specifications (2023). Construction recommendations for fill and compaction are provided in Section 7.7 in this report.

Table 6-2. Flexible Asphalt Pavement Section (Parking Lot)

Thickness (inches)	Layer	Type/Material	Compaction (percent)
2/3*	Top/Wearing Course	Asphalt Concrete	-
2	Crushed Surfacing Base Course	Mineral Aggregate per WSDOT M 41-10 9-03.9(3)	95
18/17*	Gravel Base	Mineral Aggregate per WSDOT M 41-10 9-03.10	95

* For areas of the parking lot anticipated to be traversed during the delivery and placement of prefabricated building modules, use 3 inches of asphalt concrete and reduce the gravel base thickness by 1 inch to maintain the same total section thickness.

Thickness (inches)	Layer	Type/Material	Compaction (percent)
4	Top/Wearing Course	Asphalt Concrete	-
4	Crushed Surfacing Base Course	Mineral Aggregate per WSDOT M 41-10 9-03.9(3)	95
14	Gravel Base	Mineral Aggregate per WSDOT M 41-10 9-03.10	95

Table 6-4. Rigid Pavement Section (Sidewalk)

Thickness (inches)	Layer	Type/Material	Compaction (percent)
4	Top/Wearing Course	Portland Concrete	-
2	Crushed Surfacing Base Course	Mineral Aggregate per WSDOT M 41-10 9-03.9(3)	95
14	Gravel Base	Mineral Aggregate per WSDOT M 41-10 9-03.10	95

Any existing rigid or flexible pavements that are cut for the installation of utilities must be reconstructed according to the requirements in the City of Lakewood Engineering Standards Manual (2021). Subgrade soils that are disturbed, pumped, or rutted by construction activity should be removed prior to placement

of any classified fill. Equipment should not track over or result in pumping the bottom of the excavation prior to fill placement.

6.5 Utilities

No utilities are currently connected on this site. Stub-outs may exist, but the location of these is not known.

Utilities should be installed per the local utility agencies' standards and the City of Lakewood Engineering Standards Manual (2021) considering frost depth and other constraints. Inspection of utility line subgrade should follow the requirements and standards of the City of Lakewood and the local utility owner.

All utilities should be bedded and compacted per the requirements of the pipe manufacture or local utility entity. Backfill should consist of native material or classified over the bedding, as appropriate to match soils outside the utility trench. The appropriate pavement section should be incorporated into the utility trench design depending on trench location at the site. The satisfactory performance of piped utilities is highly dependent upon the quality of soil below, along the sides, and over the pipe.

6.6 Slopes

Based on our understanding of the project scope, slopes are not anticipated for the project. Recommendations can be provided during design should they be required.

6.7 Retaining Walls and Lateral Earth Pressures

We understand retaining walls are not anticipated for this project; however, we recognize many times the site development changes such that they become necessary. We have provided the following general recommendations which can be refined if retaining walls are ultimately incorporated into the site design.

Retaining walls, including those used for basements or crawl spaces, must be designed to resist lateral earth pressures plus lateral pressure due to surcharge loads applied at the ground surface behind the wall. The magnitude of the earth pressure varies depending on permissible wall movement, type of backfill used, compaction, and drainage.

We recommend a minimum of 5 feet clean, free-draining, and properly-compacted (per our recommendations) coarse-grained soil for backfill meeting the requirements stated in WSDOT M 41-10 Section 9-03.17 Foundation Material Class A, with drainage provisions to prevent the buildup of hydrostatic pressure on the wall. All retaining wall recommendations in this report assume no hydrostatic pressures exist. Alternate recommendations can be provided, should differing materials or drainage exist. Additional lateral loads due to surface loads are not included in the equivalent fluid densities below.

The active earth pressure condition for static loading should be designed to resist the lateral earth pressure exerted by a fluid (i.e. equivalent fluid pressure) with a density of 35 pcf if the retaining wall is allowed to deflect or rotate a minimum of 0.001 times the wall height.

The at-rest pressure condition will occur if the wall is restrained at the top and cannot move sufficiently to permit the active earth pressure condition to exist. Under this condition, retaining walls should be designed to resist the lateral earth pressure exerted by a fluid with a density of 55 pcf.

The passive earth pressure condition for static loading should be designed for 250 psf/foot (pcf) if the retaining wall footing is allowed to deflect or rotate a minimum of 0.01 times the wall height. This equivalent fluid pressure includes a factor of safety of 2.0. A friction coefficient of 0.40 is recommended to be used for resistance of footings to lateral sliding. The passive pressure is permissible for use in footing design.

For seismic lateral earth pressures, we recommend a fluid density of 30 pcf be added to the active earth pressure condition. If restrained, we recommend a fluid density of 30 pcf be added to the at-rest earth pressure condition. The seismic lateral earth pressures can be treated as a triangular distribution with the application of the resultant thrust occurring at 0.4 times the wall height.

We recommend any foundation stem walls be backfilled on both sides simultaneously to prevent differential lateral loading of the foundation wall.

We note equivalent fluid pressures are not applicable to sloped backfills, surcharges, hydrostatic pressures, or braced/tie-back retaining walls. CRW can provide alternate recommendations should any of these conditions or kinds of retaining structures be present or required.

7. Construction Recommendations

7.1 Site Preparation

Existing concrete, grass, trees, and landscaping should be cleared as required to construct the proposed building and pavements. All earthwork should be performed in accordance with project specifications and with local, state, and federal laws and regulations. The City of Lakewood Engineering Standards Manual (2021) has specific requirements for soil stabilization that vary depending on the time of year. Refer to this document for guidance when planning earthwork activities.

7.2 Mitigation of Subgrade Settlement

In the vicinity of BH-01, the poorly compacted existing fill is in a loose condition based on the blow counts. If the differential settlement cannot be accommodated, one option is to overexcavate and replace the material. The existing fill contained pea gravel which is not suitable for direct re-compaction without mechanically mixing or stabilizing it. We recommend the depth of overexcavation be at least 20 feet, based on BH-01, and be thoroughly inspected to remove the poorly compacted existing fill. Native soils are medium dense to dense sand and gravel and do not require excavation and replacement. Excavated existing fill should be replaced with classified fill and compacted as discussed later in this report.

If complete overexcavation is not possible, ground improvement techniques such as vibrocompaction, stone columns, or ram aggregate piers are possible options for providing a stable subgrade to support structures. A detailed discussion of each of these options is not provided here but can be provided on request. Other options like deep dynamic compaction (DDC), grouting, or jetting are considered impractical or uneconomical for this site and therefore are not considered reasonable options.

7.3 Excavations and Subgrade Preparation

All excavations for utilities should follow proper local, state, and federal requirements including those in 29 Code of Federal Regulations (CFR) Part 1926 Occupational Safety and Health Standards Subpart P – Excavations (Occupational Safety and Health Administration [OSHA], 2020). The contractor is responsible for trench stability, worker safety, and regulation compliance as their representatives will be present on a day to day basis and can adjust efforts to obtain the needed stability.

We recommend the area surrounding any excavation be prepared to direct surface water away from the excavation and to minimize surface water or runoff from entering the excavation. This may take the form of sandbags or silt fences. Excavation and backfilling operations should be closely coordinated so that seepage and surface runoff is not allowed to collect and stand in open trenches for long periods.

Excavations above the water table may stand relatively steeply initially but fail suddenly without warning. As the in situ soils dry, they will tend to ravel and slough to their natural angle of repose, which we estimate to be about 1.7H:1V (horizontal to vertical). If surface water is allowed to enter the trench, in situ soils may soften, squeeze, slump over time or due to disturbance, to slopes of 2.5 to 3H:1V or flatter.

We recommend that the excavations be performed with equipment that minimizes disturbance of the subgrade soils. We also recommend that the exposed subgrade be evaluated by a qualified geotechnical engineer or trained inspector to identify unsuitable soils. If unsuitable soils, such as soft silts, debris-laden materials, or organics are encountered, they shall be over-excavated and replaced with engineered fill. Proof-rolling with heavy, rubber-tired construction equipment should be used for this purpose during dry weather and if access for this equipment is practical. Probing should be used to evaluate the subgrade during periods of wet weather or if access is not feasible for construction equipment. The exposed soil should be firm and unyielding, and without significant groundwater. Any soils that are disturbed, pumped, or rutted by construction activity shall be re-compacted or removed prior to placement of any classified

fill. After completion of excavation activities, excavations should be cleared of debris and any structural material used for access.

7.4 Dewatering

Groundwater conditions will vary with environmental and seasonal conditions, such as the frequency and magnitude of rainfall patterns, as well as man-made influences, such as road grades, curbs, and storm sewers. We recommend the contractor evaluate groundwater levels at the time of the construction to determine groundwater impact on the construction procedures, if necessary.

In boreholes where groundwater was encountered, it was observed below approximately 19 feet BGS in both fill and naturally-deposited soils. We do not anticipate dewatering being required during any excavations planned for construction. Surface runoff or seepage after a heavy precipitation event may cause water to pond in open excavations. Sumps and pumps are considered adequate to remove water that enters the excavation, if required.

7.5 Site Grading and Drainage

Site grading, including grade of parking areas, should be established to provide drainage of surface water and roof drainage away from proposed buildings. Grading should be designed to prevent ponding of surface water except where retention ponds or similar devices are intended. If a storm drain system is installed, site drainage should be directed toward storm drain inlets.

Based on the observed groundwater levels onsite during and after drilling and also on soil types recovered in samples, it seems probable that permeability on the site is sufficiently high to readily allow infiltration of surface water and rapid dissipation of disturbances in groundwater. Typical permeability values for the lithologies encountered (Lindeburg, 2019) and estimates using Hazen's formula with native soil properties observed on this site indicate that permeability may range from 1.4 to 270 feet per day (0.7 to 135 inches per hour). Section 7.1 of the City of Lakewood Engineering Standards Manual (2021) recommends a maximum assumed infiltration rate of 60 inches per hour for gravel and coarse sand. This assumed value may be used for site developments of less than an acre in area. A percolation test should be performed in the area to be used for infiltration to determine actual infiltration rates.

7.6 Reuse of Material

The existing gravel may potentially be reused though only meets the criteria for WSDOT Select Borrow (9-03.14(2)) in its current condition based on field observations and laboratory analysis. The presence of cobbles within five feet of ground surface is strongly indicated by drilling action in BH-03 and BH-04. The grain size distributions are within the specifications for maximum fines content for WSDOT Foundation Material Class A (9-03.17), and may meet those criteria with screening, the addition of aggregate between 3/8 and 1.5 inches in diameter, and mixing.

Any excavated on-site soils should be protected from additional moisture inputs through the use of plastic tarps or other means. Cobbles were noted in existing structural fill while drilling, though none were observed to be greater than 6 inches in size. If cobbles exceeding 6 inches in any one direction are encountered during placement of reused material, they should be removed.

When reusing material, consideration should be given to the ability to excavate, sort, and store reusable materials. This effort may be less efficient and cost more than complete removal and replacement with imported materials.

7.7 Fill and Compaction

All earthworks should be performed in accordance with the project specifications and with local, state, and federal laws and regulations.

7.7.1 Classified Fill and Compaction General Requirements

All classified fill material should be thawed, free from lumps, organics, debris, and other deleterious material and should be durable and sound. A vibratory steel drum roller should be used to compact classified fill. However, lightweight or hand-operated compactors should be used near existing structures, utilities, or new foundations to avoid damage to this infrastructure.

No hauling or grading equipment should be used in lieu of appropriate compaction equipment. Any loosening of classified fill material by hauling or other equipment should be repaired and re-compacted. The number of passes required to meet the compaction requirement will depend on the size of compaction equipment used. Each layer should be compacted as recommended in the report and field verification of compaction requirements is recommended.

Subgrade soils should be protected from freezing during construction. No frozen soil should be used as fill, nor should any fill be placed over frozen soil. Any frozen soil should be removed and replaced with appropriate classified fill prior to construction.

7.7.2 Classified Fill and Compaction

Classified fill should be placed in loose lifts not exceeding 12 inches in thickness with lift thickness adjusted based on the contractor's equipment to achieve the required compaction. Each lift of classified fill should be compacted to a minimum of 95 percent of its Modified Proctor Maximum Density, determined per ASTM D1557, unless specified elsewhere in this report.

8. Limitations and Closure

The information submitted in this report is based on our interpretation of data from a field geotechnical exploration performed for this project. The conclusions contained in this report are based on site conditions as they were observed on the drilling dates indicated. It is presumed that the exploratory borings are representative of the subsurface conditions throughout the site. Effort was made to obtain information representative of existing conditions at the site. If, however, subsurface conditions are found to differ, we should be notified immediately to review these recommendations in light of additional information.

If there is substantial lapse of time between the submittal of this report and the start of work at the site, or if conditions have changed due to natural causes or construction operations at or adjacent to the site, we recommend that this report be reviewed to determine the applicability of the conclusions considering the changed conditions and time lapse. Unanticipated soil conditions are commonly encountered and cannot fully be determined by collecting discrete samples or advancing borings. The client and contractor should be aware of this risk and account for contingency accordingly.

Samples will be retained by CRW for six months following the date on which the final report is issued. Other arrangements may be made at the client's request.

This report was prepared by CRW for use on this project only, and may not be used in any manner that would constitute a detriment to CRW. CRW is not responsible for conclusions, opinions, or recommendations made by others based on data presented in this report.

9. References

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Figure



Included in this section: 1) Site Overview and Borehole Locations

Appendix A

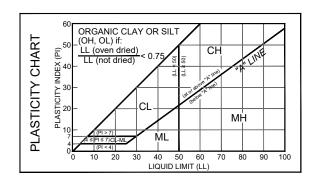
Borehole Logs



Included in this section: 1) Borehole Log Legend

2) Borehole Logs (BH-01 through BH-04)

UNIFIED	SOIL CLASSIFICATION (ASTN	1 D 2487)
GROUP SYMBOL	SOIL GROUP NAMES &	LEGEN	٩D
BLDR	COBBLES AND BOULDERS	X	
GW	WELL-GRADED GRAVEL	3	, pp
GP	POORLY GRADED GRAVEL	000	ontains and, ac sand"
GM	SILTY GRAVEL		if soil contains ≥ 15% sand, add "with sand"
GC	CLAYEY GRAVEL		- <u>_</u>
SW	WELL-GRADED SAND		
SP	POORLY GRADED SAND		ontains avel, a ravel"
SM	SILTY SAND		if soil contains 15% gravel, add "with gravel"
SC	CLAYEY SAND		м Т. С. Г.
CL	LEAN CLAY		soil s is ndy"
ML	SILT		ained (th sand er type idd "sa
OL	ORGANIC CLAY OR SILT		arse-gr add "wi vhichev 30%, <i>a</i> velly"
GW	FAT CLAY		il contains coarse-grained soil 15% to 29%, add "with sand" or n gravel" for whichever type is nent, or for ≥ 30%, add "sandy or "gravelly"
МН	ELASTIC SILT		if soil contains coarse-grained soil from 15% to 25%, acd "with sand" o "with gravel" for whichever type is "minent, or for ≥ 30%, add "sandy prominent, or "gravely"
ОН	ORGANIC CLAY OR SILT		if soi from 1 "with promir
PT	PEAT	<u>\//</u>	



COMPONENT DEFINITIONS BY GRADATION

COMPONENT	SIZE RANGE
BOULDERS	ABOVE 12 IN.
COBBLES	3 IN. TO 12 IN.
GRAVEL	3 IN. TO NO. 4 (4.76 mm)
COARSE GRAVEL	3 IN. TO 3/4 IN.
FINE GRAVEL	3/4 IN. TO NO. 4 (4.76 mm)
SAND	NO. 4 (4.76 mm) TO NO. 200 (0.074 mm)
COARSE SAND	NO. 4 (4.76 mm) TO NO. 10 (2.0 mm)
MEDIUM SAND	NO 10 (2.0 mm) TO NO. 40 (0.42 mm)
FINE SAND	NO. 40 (0.42 mm) TO NO. 200 (0.074 mm)
SILT AND CLAY	SMALLER THAN NO. 200 (0.074 mm)
SILT	0.074 mm TO 0.005 mm
CLAY	LESS THAN 0.005 mm

Gravels or sands with 5% to 12 % fines require dual symbols (GW-GM, GW-GC, GP-GM, GP-GC, SW-SM, SW-SC, SP-SM, SP-SC) and add "with clay or "with silt" to group name. If fines classify as CL-ML for GM or SM, use dual symbol GC-GM or SC-SM. <u>Optional Abverviations</u>: Lower case "s" after USCS group symbol denotes either "sandy or "with sand" and "g" denotes either "gravelly" or "with gravel." **RELATIVE DENSITY / CONSISTENCY ESTIMATE USING STANDARD PENETRATION TEST (SPT) VALUES (FROM TERZAGHI & PECK 1996)**

and "g" denotes either "gravelly	" or "with gravel."			(FRO	M TERZAGHI &	PECK 1996)						
			COHESION	ILESS SOILS ^(a)		COHESIVE SOILS(b)						
DESCRIPTIVE TE			RELATIVE DENSITY	N ₆₀ (BLOWS/FOOT) ^(c)	CONSISTENCY	N ₆₀ (BLOWS/FOOT) ^(c)	UNCONFINED COMPRESSIVE STRENGTH (TSF) ^(d)					
	```	, I	VERY LOOSE	0 - 4	VERY SOFT	0 - 2	0 - 0.25					
DESCRIPTIVE TERMS	RANGE OF		LOOSE	4 - 10	SOFT	2 - 4	0.25 - 0.50					
TRACE	0 - 5%		MED DENSE	10 - 30	MEDIUM	4 - 8	0.50 - 1.0					
FEW	5 - 10%		DENSE	30 - 50	STIFF	8 - 15	1.0 - 2.0					
LITTLE	10 - 25%		VERY DENSE	OVER 50	VERY STIFF	15 - 30	2.0 - 4.0					
SOME	30 - 45%				HARD	OVER 30	OVER 4.0					
MOSTLY	50 - 45%		drained behavior.			on possessing no characteristic	s of plasticity, and exhibiting					
	•	a		the characteristics of plasticit 1586-99 for a definition of N.		i denavior.						

(c) Refer to ASTM D 1586-99 for a definition of N. (d) Undrained shear strength,  $s_u = 1/2$  unconfined compression strength,  $U_c$ . Note that Torvane measures  $s_u$  and Pocket Pene

VS

Ω

Vane Shear

Soil Resistivity

		(d)	measure		strength, $s_u = 1/2$ uncontined compl	ression str	ssion strength, $U_c$ . Note that Torvane measures $s_u$ and Pocket Penetrometer					
		SAMPLER ABBRE					CRITE	RIA FOR DESCRIBING MOISTURE				
SS	S SPT	Sampler (2 in. OD, 140 lb hammer)		С	Core (Rock)			CONDITION (ASTM D 2488)				
SS	0 Over	size Spit Spoon (2.5 in. OD, 140 lb typ.)		ΤW	Modified Shelby		DRY	ABSENCE OF MOISTURE, DUSTY,				
HD	) Heav	y Duty Split Spoon (3 in. OD, 300/340 lb	typ.)	MS			MOIST	DRY TO THE TOUCH DAMP BUT NO VISIBLE WATER				
BD	) Bulk	Drive (4 in. OD, 300/340 lb hammer typ.	)	GP Geoprobe			VISIBLE FREE WATER, USUALLY					
CA	Cont	inuous Core (Soil in Hollow-Stem Auger)	)	AR	Air Rotary Cuttings		WET	SOIL IS BELOW WATER TABLE				
G	Grab	Sample from surface / testpit		AG	Auger Cuttings		L					
		LA	BORA	TOR	Y TEST ABBREVIATI	IONS						
Г	AL	Atterberg Limit	PI	PI	lastic Index	TS	Thaw	Consolidation				
	Consol	Consolidation	PID	Pł	hotoionization Detector	TV	Torva	ine				
	LMA	Limited Mechanical Analysis	Pro	c Pr	roctor	TXC	D Cons	olidated Drained Triaxial				
	MA	Sieve and Hydrometer Analysis	PP	Po	ocket Penetrometer	TXC	U Cons	olidated Undrained Triaxial				
	MC	Moisture Content	P20	0 Pe	ercent Fines (Silt & Clay)	TXU	U Unco	nsolidated Undrained Triaxial				

Sieve Analysis

Specific Gravity

SA

SpG

Non-plastic NP OLI Organic Loss



### LEGEND: SOIL CLASSIFICATION AND ABBREVIATIONS

à tech end\Geot 0 Template\Borehole Report Geotechnical Geotechnical\CRW References M: \Engineering NAMF: FILE

1. DESCRIBE SOIL	-	CLASS	IFY SOI	L BY THE	UNIFIED SOIL		
INDEPENDENT O FROZEN STATE	F	C	LASSIF	ICATION S	SYSTEM		
	MAJO	R GROUP			SUBGROL	JP	ICE BONDING SYMBOL
	DESCRIPTION	DESIGN	ATION	DES	CRIPTION	DESIGNATION	No ice-bonded soil
	Segregated			Poorly b	onded of friable	N _f	observed
	ice not visible by eye	N		Well	No excess ice	Nbn	Poorly bonded or friable
2. MODIFY SOIL				bonded	Excess ice	Nbe	
DESCRIPTION B DESCRIPTION OI FROZEN SOIL					I ice crystals or clusions	Vx	Well bonded
	Segregated ice			Ice coati	ngs on particles	Vc	DEFINITIONS
	visible by eye (ice less than 25 mm thick)				n or irregularly ice formations	Vr	<u>Candled Ice</u> is ice which has rotted or otherwise formed into long columnar crysta very loosely bonded together.
					ed or distinctly ice formations	Vs	<u>Clear Ice</u> is transparent and contains only a moderate number of air bubbles.
				Uniform	y distributed ice	Vu	<u>Cloudy Ice</u> is translucent, but essentially so and non-pervious.
3. MODIFY SOIL DESCRIPTION BY DESCRIPTION OI	5	ICE		soil inclusions	ICE+soil type	<u>Friable</u> denotes a condition in which materi easily broken up under light to moderate pressure.	
SUBSTANTIAL IC STRATA				Ice witho	ut soil inclusions	ICE	<u>Granular Ice</u> is composed of coarse, more less equidimensional, ice crystals weakly bonded together.
	FROST DESIGN		SIFIC				Ice Coatings on particles are discernible la
FROST GROUP ⁽²⁾	GENERAL SOIL T		% FIN 0.02	ER THAN mm BY EIGHT		AL USCS CLASS	of ice found on or below the larger soil par in a frozen soil mass. They are sometimes associated with hoarfrost crystals, which h grown into voids produced by the freezing
NFS ⁽³⁾	(a) Gravels Crushed stone Crushed rock	•		) - 1.5	GW, GP		action. <u>Ice Crystal</u> is a very small individual ice par visible in the face of a soil mass. Crystals r
	(b) Sands		0-3 SW, SP			be present alone or in a combination with o ice formations.	
PFS ⁽⁴⁾ [MOA NFS] [FAA NFS]	(a) Gravels Crushed stone Crushed rock			0 - 3 .5 - 3		v, gp	<u>Ice Lenses</u> are lenticular ice formations in s occurring essentially parallel to each other generally normal to the direction of heat los and commonly in repeated layers.
	(b) Sands			3 - 10	SV	V, SP	Ice Segregation is the growth of ice as dist
[MOA F-2] [FAA FG-2] S1 [MOA F-1] [FAA FG-1]	Gravelly soils			3 - 6	GW, GP, GV	V-GM, GP-GM, C, GP-GC	lenses, layers, veins and masses in soils, commonly but not always oriented normal direction of heat loss.
S1 [MOA F-2] [FAA FG-2]	Sandy soils			3 - 6	SW, SP, SV	V-SM, SP-SM, C, SP-SC	<u>Massive Ice</u> is a large mass of ice, typically nearly pure and relatively homogeneous.
F1 ⁽⁵⁾ [MOA F-1] [FAA FG-1]	Gravelly soils		6	6 - 10		1-GC, GW-GM, V-GC, GP-GC	Poorly-Bonded signifies that the soil particl are weakly held together by the ice and the frozen soil consequently has poor resistan chipping or breaking.
F2 ⁽⁵⁾	(a) Gravelly soi	ls	1	0 - 20	GW, GP, GW-GM, GP-GM, GW-GC, GP-GC		Porous Ice contains numerous void, usuall interconnected and usually resulting from
[MOA F-2] [FAA FG-2]	(b) Sands		6	6 - 15	SM, SW-SM, SP-SM, SC, SW-SC, SP-SC, SM-SC		melting at air bubbles or along crystal inter from presence of salt or other materials in water, or from the freezing of saturated sm
F3 ⁽⁵⁾	(a) Gravelly soi		0	ver 20	GM, GO	C, GM-GC	Though porous, the mass retains its struct unity.
[MOA F-3] [FAA FG-3]	(b) Sands, except very sands	except very fine silty Over 15 S sands		SM, SC	C, SM-SC	Thaw-Stable frozen soils do not, on thawin	
	(c) Clays, PI>1	2			CL	., CH	show loss of strength below normal, long-t
	(a) Silts				ML, M	H, ML-CL	thawed values nor produce detrimental settlement.
<b>-</b> (5)	(b) Very fine silty s	sands	0	ver 15		C, SM-SC	Thaw-Unstable frozen soils show on thawi
F4 ⁽⁵⁾ [MOA F-4] [FAA FG-4]	(c) Clays, Pl≤1	2			CL,	ML-CL	significant loss of strength below normal, long-time thawed values and/or significant
	(d) Varved clays or other banded sedimer	•				red with ML, MH, SC, or SM-SC	settlement, as a direct result of the melting the excess ice in the soil.

(2) DSACE nos groups directly correspond to insignoups in Maintopainy of Antonradge (MOA) Design Criteria Maintain (DCM), Federal Aviation AC frost groups come from Table 2-2 in Section 2.5.4 of Advisory Circular (AC) 150/5320-6G, Airport Pavement Design and Evaluation (June, 2021).
 (3) Non-frost susceptible
 (4) Possibly frost susceptible, requires lab test for void ratio to determine frost design classification.
 (5) Consistent with MAA Definition.



M: \Fn

FILE NAME:

### LEGEND: FROZEN SOIL CLASSIFICATION

	CRW Engineering Group, Inc. 3940 Arctic Blvd Ste. 300 Anchorage, Alaska 99503 Telephone: 907-562-3252 Fax: 907-561-2273			BORE	HOLE BH-0 PAGE 1 OF
	Work	PROJECT NAME Lakewood	od Interim Libra	ary	
PROJECT NUMBI	ER 52501.00	PROJECT LOCATION Lak	ewood, Wash	ington	
DATE STARTED	<u>01/12/23</u> COMPLETED <u>01/12/23</u>	GROUND ELEVATION			
DRILLING CONTR	RACTOR Holt Services, Inc.	GROUND WATER LEVELS	:		
DRILLING METHO	OD Hollow-Stem Auger	$\overline{igsiresizet}$ at time of drillin	<b>IG</b> 20.00 ft		
	CHECKED BY <u>SMH</u>	$\Psi$ at end of drilling $\Psi$ after drilling <u>1</u>			
DEPTH (ft) U.S.C.S. GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER RECOVERY % (RQD) FIELD BLOW COUNTS	(N VALUE) POCKET PEN. (psf) ICE BOND	PID OTHER TESTS	▲ FIELD N VALUE 10 20 30 40 PL MC LL 10 20 30 40
0 - GP- 0 GM 0 0	POORLY GRADED GRAVEL WITH SILT AND SAND, (GP-GM) 63% gravel, 32% sand, 5% fines Gray, moist, no odor. Angular sand, fine to coarse. Subangular to angular gravel up to 2", some elongate. Likely fill.			LMA	
	POORLY GRADED GRAVEL WITH SILT AND SAND, (GP-GM) 67% gravel, 28% sand, 5% fines Gray, moist, no odor. Rounded gravel up to 0.5", subangular to rounded gravel up to 1.5" appears to have different provenance. Likely different types of fill.	SS 67 (13		SA	0
5	POORLY GRADED GRAVEL WITH SAND, (GP) 78% gravel, 20% sand, 2% fines Gray, moist to wet, no odor. Fine to coarse sand. Subangular to rounded gravel up to 1.5". Likely fill.			LMA	0 •
		SS S4 33 3-5- (11		LMA	0
	81% gravel, 17% sand, 2% fines	SS 33 4-2- (4)		SA	<u>○</u>
- GP - - - - - - - - - - - - - - - - - -					
	Gravel up to 0.5". Likely fill, cuttings from 2.5 to 20 feet BGS and sample at this depth appear to be predominar pea gravel.	tly $SS$ 22 5-3- (7)			
20					

(Continued Next Page)



CRW Engineering Group, Inc. 3940 Arctic Blvd Ste. 300

# **BOREHOLE BH-01**

PAGE 2 OF 2

CLIENT BuildingWork

CRW MOA LOG - CRW_DATATEMPLATE_20190115.GDT - 04/12/23 11:46 - 52501 LAKEWOOD.GPJ

PROJECT NUMBER 52501.00

PROJECT NAME _Lakewood Interim Library

PROJI	ECT N	IUMBER	_52501.00 PRO	JECT LO	CATIO	N Lakewo	od, Wa	ashir	igton		
05 DEPTH (ft)	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	FIELD BLOW COUNTS (N VALUE)	POCKET PEN. (psf)	ICE BOND	DIA	OTHER TESTS	▲ FIELD N VALUE ▲ 10 20 30 40 PL MC LL 10 20 30 40
20	GP		POORLY GRADED GRAVEL WITH SAND, (GP) 81% gravel, 18% sand, 1% fines Brown, wet, no odor. Fine to coarse sand. Subangular to rounded gravel up to 1.5", likely larger in situ. Rounded gravel up to 3" observed in cuttings. 81% gravel, 18% sand, 1% fines SILTY SAND WITH GRAVEL, (SM) 33% gravel, 41% sand, 26% fines Gray, moist to wet, no odor. Fine to coarse sand. Subrounded to rounded gravel up to 1". Likely larger grave or cobbles based on drilling action and blow count.	SS S7 SS S8 S8	50	5-14-21 (35) 6-10-19 (29) 25-55/2"				LMA	
			Fine-grained portion of the sample was soft, but overall mechanical behavior of this interval is likely controlled by the coarse granular component. Bottom of borehole at 30.7 feet. Notes: Completed as piezometer to 30.5 feet BGS. 2" PVC with bottom 15 feet hand slotted. Steel flushmount, unique well ID BPW-491-MW1.								

		R\	CRW Engineering Group, Inc. 3940 Arctic Blvd Ste. 300 Anchorage, Alaska 99503 Telephone: 907-562-3252 Fax: 907-561-2273							BC	DRE	Ю		BH GE 1		
			ork	PROJE	CT NA	ME _L	akewood In	terim L	ibrar	у						
			_52501.00													
			1/12/23 COMPLETED 01/12/23													
ORILL	ING (	CONTRA	CTOR _ Holt Services, Inc.	GROUN	DWA	TER LE	EVELS:									
ORILL	ING I	NETHOD	Hollow-Stem Auger	${ar ar \Sigma}$ a	т тімі	E OF D	RILLING _	20.00	ft							
OGG	ED B	Y AFS	CHECKED BY SMH				RILLING _									
NOTE	s			Α	FTER	DRILL	NG									
DEPTH (ft)	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY % (RQD)	FIELD BLOW COUNTS (N VALUE)	POCKET PEN. (psf)	ICE BOND	PID	OTHER TESTS			N VA 0 30		
0	Ď	Ъ.			SAMI	REC(	E E	POC	ICE		0-	F	²L I 	MC 30		)
_			WELL GRADED GRAVEL WITH SAND, (GW) 50% gr 45% sand, 5% fines Gray-brown to brown, moist, no odor. Fine to coarse sa Subangular to rounded gravel up to 1.5". Visual classification in field.		SS S1	50	8-17-24 (41)	-				0				<b>k</b>
-	GW			X	SS S2		5-22-25	-				0				•
_				_		39	(47)	-								
5			WELL GRADED GRAVEL WITH SILT AND SAND, (GW-GM) 58% gravel, 37% sand, 5% fines Brown, moist to wet, no odor. Fine to coarse sand. Subangular to rounded gravel up to 1.5", likely larger in		SS S3	50	6-18-19 (37)	-			SA	0				
_			Rounded cobbles up to 8" observed in cuttings.		] ] SS			-				0				
-					<u>\$4</u>	28	7-15-13 (28)	-						<b>A</b>		
10				X	SS S5		10-11-14	-				0				-
_						50	(25)	-								
-	GW- GM															
-																,
-				X	SS S6	56	18-23-30 (53)					O				
_																•
-																
20			7									:	:		÷	



CRW Engineering Group, Inc. 3940 Arctic Blvd Ste. 300

# **BOREHOLE BH-02**

PAGE 2 OF 2

CLIENT BuildingWork

PROJECT NAME Lakewood Interim Library

PROJ	ECT N	IUMBE	R_52501.00 PR	OJ	ECT LO	CATIO	N Lakewo	od, W	ashir	ngton				
05 DEPTH (ft)	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY % (RQD)	FIELD BLOW COUNTS (N VALUE)	POCKET PEN. (psf)	ICE BOND	DID	OTHER TESTS	PL	20 30	
	SP		POORLY GRADED SAND WITH GRAVEL, (SP) 48% gravel, 50% sand, 2% fines Brown, wet, no odor. Fine to coarse sand. Subangular to rounded gravel up to 1".		SS S7	² 39	14-11-11 (22)	-			LMA	0		
    30	GP- GM	≠ ∞ ∞ ∞ ∞ ∞ ∞ ∞ ∞ ∞ ∞ ∞ ∞ ∞ ∞ ∞ ∞ ∞ ∞ ∞	POORLY GRADED GRAVEL WITH SILT AND SAND, (GP-GM) 65% gravel, 20% sand, 15% fines Brown, wet, no odor. Rounded gravel up to 1". SILTY GRAVEL WITH SAND, (GM) 44% gravel, 35% sand, 21% fines Brown, moist, no odor. Rounded gravel up to 1".		SS S8A SS S8B	10	15-29-39 (68)	-			LMA	0		>>
	SP- SM	0	POORLY GRADED SAND WITH SILT AND GRAVEL, (SP-SM) 40% gravel, 50% sand, 10% fines Brown to gray, moist, no odor. Fine to coarse sand. Subrounded gravel up to 1". Bottom of borehole at 30.9 feet. Notes: Backfilled with cuttings.		SS S9	100	22-55/5"					0		>>

			CRW Engineering Group, Inc. 3940 Arctic Blvd Ste. 300 Anchorage, Alaska 99503 Telephone: 907-562-3252 Fax: 907-561-2273						DU	JRE	PAGE 1 OF 1
			Fax: 907-561-2273	PROJECT N		akewood Ir	terim I	ibrar	7.7		
			2_52501.00								
			11/12/23 <b>COMPLETED</b> 01/12/23								
			CTOR Holt Services, Inc.								
			Hollow-Stem Auger			RILLING	Nowo	or of	beorve	d	
			CHECKED BY SMH			_					
DEPTH (ft)	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	FIELD BLOW COUNTS (N VALUE)	POCKET PEN. (psf)	ICE BOND	PID	OTHER TESTS	▲ FIELD N VALUE ▲ 10 20 30 40 PL MC LL
0			POORLY GRADED GRAVEL WITH SAND, (GP) 60%	X ss	;						10 20 30 40 O: : : :
-			gravel, 35% sand, 5% fines Brown to dark brown, moist, no odor. Fine to coarse san Rounded gravel up to 1.5", likely larger in situ. Visual classification in field. Rig repositioned slightly after auge deviated from vertical while penetrating a resistant layer ft BGS.	r		6-7-9 (16)	-				
-	GP		11 803.			6-8-17 (25)	_				o ▲
5	 SP		POORLY GRADED SAND WITH GRAVEL, (SP) 40% gravel, 56% sand, 4% fines I Brown, moist, no odor. Fine to coarse sand. Subangular I rounded gravel up to 1.25", likely larger gravel and cobbl	to	50	10-17-25 (42)	_			LMA	0
-			in situ based on drilling action. Auger grinding 4 to 7.5 ft BGS. POORLY GRADED GRAVEL WITH SAND, (GP) 76% gravel, 21% sand, 3% fines Brown, moist, no odor. Fine to coarse sand. Subangular rounded gravel up to 2", likely larger gravel and cobbles i	to SS		5-12-35 (47)	-				0
-			Auger grinding 9 to 10 ft BGS.			(47)	_				
_	GP					12-32-17 (49)				LMA	0
-											
-											
						30-21-30 (51)					O.
			Bottom of borehole at 16.5 feet. Notes: Backfilled with cuttings.								

Г

	C	R	CRW Engineering Group, Inc. 3940 Arctic Blvd Ste. 300 Anchorage, Alaska 99503 Telephone: 907-562-3252 Fax: 907-561-2273							BC	DRE	HOLE BH-04 PAGE 1 OF 1		
		uildingW		PROJI			akewood In	terim L	.ibrar	у				
PROJ		UMBEF	8_52501.00	PROJECT LOCATION Lakewood, Washington										
				GROUND ELEVATION										
			CTOR Holt Services, Inc.											
			CHECKED BY <u>SMH</u>											
DEPTH (ft)		GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY % (RQD)		POCKET PEN. (psf)		DID	OTHER TESTS	▲ FIELD N VALUE ▲ 10 20 30 40 PL MC LL		
	_		WELL GRADED GRAVEL WITH SAND, (GW) 63% gra 33% sand, 4% fines Dark brown, moist, no odor. Medium to coarse sand. Subrounded to rounded gravel up to 1.5", likely larger in situ. Cobbles up to 5" observed in cuttings. Rig reposition	ned	SS S1	39	7-8-7 (15)				SA	10 20 30 40 ©		
	-		slightly after auger deviated from vertical while penetrati resistant layer at 3 ft BGS. 67% gravel, 30% sand, 3% fines	ing a	SS S2	33	4-4-5 (9)	-			LMA	0		
	- GW				≤ SS S3	17	5-3-3 (6)	-				•		
	_				≤ SS S4	60	55/5"	-				O >>		
	-	3000 0000 0000 00000000000000000000000	POORLY GRADED GRAVEL WITH SILT AND SAND, (GP-GM) 53% gravel, 42% sand, 5% fines Brown, moist, no odor. Fine to coarse sand. Angular to rounded gravel up to 2", likely larger gravel and cobbles situ based on drilling action. Auger grinding throughout t interval.	in this	SS S5	28	20-19-19 (38)	_			LMA	0		
	GP- GM			K	1			_						
	_		Bottom of borehole at 16.5 feet.	2		28	4-8-19 (27)					0		
			Notes: Backfilled with cuttings.											

# Appendix B

Laboratory Results



ATL

Mate	erial Test F	<b>≀eport</b>	Issue No: 1					
Client:	: CRW Engineering Group, Inc 3940 Arctic Blvd., Ste. 300 Anchorage, AK, 99503		Project Code: 230782 CC: CRW Inc Maria Kampsen	The results contained below pertain only to the items tested below. This report should not be reproduced, except in full, without the prior written approval of Alaska Testlab or the agency.				
Project:	Lakewood				Marchanpser			
	Anchorage, AK, 99503			Boviowed By: Mari				
	52501.00				ior Engineer i/2023			
Samp	le Details							
Sample Client S Date Sa	Sample ID		23-0105-S01 BH-01 Sa1	23-0105-S02 BH-01 Sa2	23-0105-S03 BH-01 Sa3			
	Test Results							
Descrip	otion	Method		Results		Limits		
Water C	content (%)	ASTM D2216	5	4	3			
Date Tes	sted		1/18/2023	1/18/2023	1/18/2023			
Tested E	Зу		Tammy Lozano	Tammy Lozano	Tammy Lozano			
Group C		ASTM D2487	GP-GM	GP-GM	GP			
Group N			Poorly graded gravel with silt and sand	Poorly graded gravel with silt and sand	Poorly graded gravel with sand			
•	g Limits Estimated		Yes	Yes	Yes			
Gravel (	· · · · ·		63		78			
Sand (%	·		32		20			
Fines (%	-		5		2			
Tested E	Зу	ASTM D2487	Karen Jackson		Karen Jackson			
Method		ASTM D6913		A				
•	tion Method			Oven Dry				
	site Sieving?			Yes				
	ing Sieve(s)			No. 4				
Cu		ASTM D2487		13.51				
Cc				3.37				

ATL

Mate	erial Test F	Report		Report No: A Issue No: 1					
Client:	CRW Engineering Group, Inc 3940 Arctic Blvd., Ste. 300 Anchorage, AK, 99503		Project Code: 230782 CC: CRW Inc Maria Kampsen	The results contained below pertain only to the items tested below. This report should not be reproduced, except in full, without the prior written approval of Alaska Testlab or the agency.					
Project:	Lakewood				Man Etarpsen				
	Anchorage, AK, 99503			Deviewed Dw. Me					
	52501.00			Reviewed By: Ma Title: Se	-				
					nior Engineer 25/2023				
Samp	le Details								
Sample	) ID		23-0105-S04	23-0105-S05	5 23-0105-S06				
	Sample ID		BH-01 Sa4	BH-01 Sa5	5 BH-01 Sa6				
Date Sa									
	Test Results								
Descrip	otion	Method		Results		Limits			
Water C	ontent (%)	ASTM D2216	4	4	4 4				
Date Te	sted		1/18/2023	1/18/2023	3 1/18/2023				
Tested E	Зу		Tammy Lozano	Tammy Lozano	D Tammy Lozano				
Group C	ode	ASTM D2487	GP	GF	0				
Group N	lame		Poorly graded gravel with sand	Poorly graded gravel with sand	t				
Atterber	g Limits Estimated		Yes	Yes	6				
Gravel (	,		72						
Sand (%	·		26						
Fines (%	,		2						
Tested E	Зу	ASTM D2487							
Method		ASTM D6913		Ą					
-	tion Method			Oven Dry					
	ite Sieving?			Yes					
-	ng Sieve(s)			No. 4					
Cu		ASTM D2487		3.04					
Cc				1.56	j				

ATL

	est Report		Report No: ASI Issue No: 1		
Client: CRW Enginee 3940 Arctic B Anchorage, A Project: Lakewood		Project Code: 230782 CC: CRW Inc Maria Kampsen		ain only to the items tested below. This repo It the prior written approval of Alaska Testlab	
Anchorage, A 52501.00	K, 99503		Reviewed By: Maria Title: Senio Date: 1/25/2	r Engineer	
Sample Details					
Sample ID Client Sample ID Date Sampled		23-0105-S07 BH-01 Sa7	23-0105-S08 BH-01 Sa8	23-0105-S09 BH-01 Sa9	
Other Test Res	ults				
Description	Method		Results		Limits
Water Content (%) Date Tested Tested By	ASTM D2216	12 1/18/2023 Tammy Lozano	18 1/18/2023 Tammy Lozano	10 1/18/2023 Tammy Lozano	
Group Code Group Name Atterberg Limits Estima	ASTM D2487		GP Poorly graded gravel with sand Yes	SM Silty sand with gravel 0	
Liquid Limit Plasticity Index Gravel (%)			81	0 33	
Sand (%) Fines (%) Tested By	ASTM D2487		18 1 Karen Jackson	41 26 Karen Jackson	

ATL

					lss	Report No: MAT:23-0105-S02 Issue No: 1				
Client:	CRW Engineerin 3940 Arctic Blvd Anchorage, AK,	., Ste. 300	-	t Code: 230782 C: CRW Inc Maria Kampsen	2			iain only to the items tested below. Thi It the prior written approval of Alaska T		
Project:	Lakewood							Man Aprpsen		
	Anchorage, AK,	99503				Bovi	iowod Py: Moria	E Kompson		
	52501.00					Title	iewed By: Maria Senio	r Engineer		
						Date				
Samp	le Details							ize Distribution		
Sample Client \$	e ID Sample ID	23-0105-S02 BH-01 Sa2					Method: Drying By: Date Tested: Tested By:	ASTM D6913 Oven 1/20/2023 Karen Jackson		
							Sieve Size 3in 2in 1½in 1in ¾in ½in	<b>% Passing</b> 100 100 100 98 90 79	Limits	
Other	Test Resu	lts					3/8in	68		
Descri		Meth		Result	Limits		No.4	32.9		
	Content (%)	ASTI	M D2216	4			No.10	17		
Date Te			Tam	1/18/2023			No.20	11		
Tested		ACT	1 am M D2487	my Lozano			No.40	9		
Group				GP-GM			No.60 No.100	7		
Group I		Poorly graded gra	iver with si	it and sand Yes			No.200	6 5		
Method	rg Limits Estima		M D6913	A			10.200	5		
	ation Method	ASTI	VI DO915	Oven Dry						
	site Sieving?			Yes						
	ting Sieve(s)			No. 4						
Cu		ASTI	M D2487	13.51						
Cc		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	DETOT	3.37						
Date Te	ested			1/20/2023						
							Chart			
								Diameter		
							100 60	20 6 2 6	00 200 100 50 —— µm —————————————————————————————————	
							100 🕂 🖶 🌩	<b>₽</b> └┓╎╶╎///////////////////////////////////	+++++++++++++++++++++++++++++++++++++++	
							90 (ssem Ad) buissed 40 50 40 20 10			
							0 Sieve Size 3" 2"	1" 1/2" #4 #10 #20	#40 #100	
L										

Soil Classification of Fines (-#200) in Sieve Analyses Assumed Unless Verified by Additional Testing No Plasticity Index Test Performed

ATL

Material Test Report					Report No: MAT:23-0105-S05 Issue No: 1					
Client:	CRW Engineerin 3940 Arctic Blvd Anchorage, AK,	., Ste. 300	-	t Code: 230782 C: CRW Inc Maria Kampsen				iain only to the items tested below. T		
Project:	Lakewood							Man Aprpsen	)	
	Anchorage, AK,	99503				Revi	ewed By: Maria	E Kampsen		
	52501.00					Title	: Senio	or Engineer		
						Date	e: 1/25/2	2023		
Samp	le Details							ize Distributio	n	
Sample Client S	∋ ID Sample ID	23-0105-S05 BH-01 Sa5					Method: Drying By: Date Tested: Tested By:	ASTM D6913 Oven 1/20/2023 Karen Jackson		
							Sieve Size 3in 2in 1½in 1in ¾in	% Passing 100 100 100 100 90	Limits	
Other	Test Resu	lts					½in 3/8in	88 81		
Descrip	otion	Metl	nod	Result	Limits		No.4	19.0		
Water C	Content (%)	AST	M D2216	4			No.10	7		
Date Te				1/18/2023			No.20	5		
Tested			Tam	my Lozano			No.40	3		
Group (			M D2487	GP			No.60	2		
Group I			aded grave	el with sand			No.100	2		
	rg Limits Estima			Yes			No.200	2		
Method		AST	M D6913	A						
	ation Method			Oven Dry						
	site Sieving?			Yes						
	ting Sieve(s)	ACT		No. 4						
Cu Cc		AST	M D2487	3.04 1.56						
Date Te	eted			1/20/2023						
	sieu			1/20/2023						
							Chart			
							onart			
							100 60	Diameter 20 6 2	600 200 100 50	
								mm+	μm	
							100 90 (ssem (a) buissed 30 40 80 50 40 80 80 80 80 80 80 80 80 80 80 80 80 80			
							Sieve Size 3" 2"	1" 1/2" #4 #10 #2	20 #40 #100	
L										

Soil Classification of Fines (-#200) in Sieve Analyses Assumed Unless Verified by Additional Testing No Plasticity Index Test Performed

ATL	

Material [·]	<b>Test Report</b>	Rep Issu	Report No: ASM:23-0106 Issue No: 1					
Client: CRW Engineering Group, Inc 3940 Arctic Blvd., Ste. 300 Anchorage, AK, 99503		Project Code: 230 CC: CRW Inc Maria Kamps	reproduc	The results contained below pertain only to the items tested below. This report should not be reproduced, except in full, without the prior written approval of Alaska Testlab or the agency.				
Project: Lakewood				Par	Ampsen			
Anchorage 52501.00	, AK, 99503		Revie Title: Date:	5	•			
Sample Detai	ls							
Sample ID Client Sample ID Date Sampled		23-0106-S01 BH-02 Sa1	23-0106-S02 BH-02 Sa2	23-0106-S03 BH-02 Sa3	23-0106-S04 BH-02 Sa4			
Other Test Re	esults							
Description	Method		Res	ults		Limits		
Water Content (%) Date Tested Tested By	ASTM D2216	6 1/18/2023 Tammy Lozano	6 1/18/2023 Tammy Lozano	6 1/18/2023 Tammy Lozano	6 1/18/2023 Tammy Lozano			
Group Code Group Name Atterberg Limits Est	ASTM D2487	7		GW-GM Well-graded gravel with silt and sand Yes	·			
Method	ASTM D6913	3		A				
Preparation Method Composite Sieving? Separating Sieve(s)	,			Oven Dry Yes No. 4				
Cu Cc	ASTM D2487	7		33.58 1.26				

ATL	

viate	erial Test F	keport				ort No: ASM:23-0 e No:  1		
Client:	CRW Engineering Grou 3940 Arctic Blvd., Ste. 3		Project Code: 23078	82	The result	is contained below pertain only to t id, except in full, without the prior v	he items tested below. This repor	t should not be or the agency.
	Anchorage, AK, 99503		Maria Kampser	n		1		
Project:	Lakewood					1 an	Etapser	
	Anchorage, AK, 99503				Reviev	ا wed By: Maria E Kam	insen	
	52501.00				Title: Date:	Senior Engin 1/25/2023		
Samp	le Details			-				
Sample Client S Date Sa	Sample ID		23-0106-S05 BH-02 Sa5	23-0106- BH-02		23-0106-S07 BH-02 Sa7	23-0106-S08 BH-02 Sa8A	
	Test Results							
Descrip	otion	Method			Resu	lts		Limits
	ontent (%)	ASTM D2216	6		8	11	15	
Date Tes			1/18/2023	1/18/2		1/18/2023	1/18/2023	
Tested E		A OTH A DO 10-	Tammy Lozano	Tammy Loz	zano	Tammy Lozano	Tammy Lozano	
Group C Group N Atterberg Gravel ( ⁶ Sand (% Fines (%	ame g Limits Estimated %) )	ASTM D2487				SP Poorly graded sand with gravel Yes 48 50 2		
Tested E	3 <b>у</b>	ASTM D2487				Karen Jackson		

Material Test F	Report			Report No Issue No:	: ASM:23-0106 1	
Client: CRW Engineering Group 3940 Arctic Blvd., Ste. 3 Anchorage, AK, 99503	o, Inc	Project Code: 2307 CC: CRW Inc Maria Kampse		The results contained	below pertain only to the items tested below. This full, without the prior written approval of Alaska Te	report should not be stlab or the agency.
Project: Lakewood					Maretanpser	
Anchorage, AK, 99503 52501.00				Reviewed By: Title: Date:	Maria E Kampsen Senior Engineer 1/25/2023	
Sample Details						
Sample ID Client Sample ID Date Sampled		23-0106-S09 BH-02 Sa8B	23-0106 BH-02			
Other Test Results						
Description	Method			Results		Limits
Water Content (%) Date Tested Tested By	ASTM D2216	8 1/18/2023 Tammy Lozano	1/18/2 Tammy Lo:			
Group Code	ASTM D2487	GM		Lano		
Group Name Liquid Limit Plasticity Index Gravel (%) Sand (%) Fines (%) Tested By	ASTM D2487	Silty gravel with sand 0 0 44 35 21 Karen Jackson				
Comments Soil Classification of Fines (-#200)	in LMAs Assum	ed Unless Verified by	Additional Te	sting		

ATL

Material Test Report						Report No: MAT:23-0106-S03 Issue No: 1				
Client:	CRW Engineering 3940 Arctic Blvd. Anchorage, AK, S	, Ste. 300	-	C: CRW Inc Maria Kampsen				ain only to the items tested below. This it the prior written approval of Alaska T		
Project:	Lakewood							Man Apropser		
	Anchorage, AK, §	99503				Revi	ewed By: Maria	E Kampsen		
	52501.00					Title	: Senio	or Engineer		
						Date	e: 1/25/2	2023		
_	le Details							ize Distribution		
Sample Client S	e ID Sample ID	23-0106-S03 BH-02 Sa3					Method: Drying By: Date Tested: Tested By:	ASTM D6913 Oven 1/20/2023 Karen Jackson		
							Sieve Size 3in 2in 1½in 1½in ¾in ½in	<b>% Passing</b> 100 100 100 93 80 64	Limits	
Other	Test Resul	ts					3/8in	57		
Descri			thod	Result	Limits		No.4	41.6		
	Content (%)	AS	TM D2216	6			No.10	30		
Date Te			-	1/18/2023			No.20	19		
Tested		4.0	1 am TM D2487	my Lozano			No.40	12		
Group				GW-GM			No.60	9		
Group I		Well-graded g	ravel with si				No.100	7		
	rg Limits Estimat			Yes			No.200	5		
Method		A5	TM D6913							
	ation Method			Oven Dry Yes						
	site Sieving? ting Sieve(s)			No. 4						
Cu	ung Sieve(s)	45	TM D2487	33.58						
Cc		70	TW D2407	1.26						
Date Te	ested			1/20/2023						
	53100			1/20/2023						
							Chart			
								Diameter		
							100 60	20 6 2 6	00 200 100 50 —— µm —————————————————————————————————	
							100 🔫 🖷			
							90 90 40 50 50 40 50 30 20 80 80 80 90 90 90 90 90 90 90 90 90 90 90 90 90			
							10		***	
							Sieve Size 3" 2"	1" 1/2" #4 #10 #20	#40 #100	

Soil Classification of Fines (-#200) in Sieve Analyses Assumed Unless Verified by Additional Testing No Plasticity Index Test Performed

ATL
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	erial Test F		Report No: ASM:23-0107 Issue No: 1				
Client: Project:	CRW Engineering Group 3940 Arctic Blvd., Ste. 3 Anchorage, AK, 99503 Lakewood		Project Code: 230782 CC: CRW Inc Maria Kampsen	The results contained below pertain only to the items tested below. This report should not be reproduced, except in full, without the prior written approval of Alaska Testlab or the agency.			
	Anchorage, AK, 99503 52501.00			Reviewed By: Maria Title: Senio Date: 1/25/	or Engineer		
amp	le Details						
Sample Client S			23-0107-S01 BH-03 Sa1	23-0107-S02 BH-03 Sa2	23-0107-S03 BH-03 Sa3		
	Test Results						
Descrip	otion	Method		Results		Limits	
Vater C Date Tes Fested E		ASTM D2216	7 1/18/2023 Tammy Lozano	8 1/18/2023 Tammy Lozano	6 1/18/2023 Tammy Lozano		
Group C Group N	ode ame g Limits Estimated %)	ASTM D2487			SP Poorly graded sand with gravel Yes 40 56 4		

AIL

	erial Test F			Report No: ASI Issue No: 1		
Client:	CRW Engineering Group 3940 Arctic Blvd., Ste. 3 Anchorage, AK, 99503 Lakewood		Project Code: 230782 CC: CRW Inc Maria Kampsen	The results contained below per reproduced, except in full, without	tain only to the items tested below. This report It the prior written approval of Alaska Testlab of	t should not be or the agency.
Project:	Lakewood				Marenper	
	Anchorage, AK, 99503 52501.00			Reviewed By: Maria Title: Senic Date: 1/25/2	or Engineer	
Samp	le Details					
Sample Client S Date Sa	Sample ID		23-0107-S04 BH-03 Sa4	23-0107-S05 BH-03 Sa5	23-0107-S06 BH-03 Sa6	
Other	Test Results					
Descrip		Method		Results		Limits
Water C Date Te Tested B		ASTM D2216	7 1/18/2023 Tammy Lozano	6 1/18/2023 Tammy Lozano	8 1/18/2023 Tammy Lozano	
Group C Group N	Code lame g Limits Estimated %)	ASTM D2487		GP Poorly graded gravel with sand Yes 76 21 3		
Tested I	зу	ASTM D2487		Karen Jackson		

ATL

Mat	erial Test F	Report	Report No: A Issue No: 1				
Client:	CRW Engineering Grou 3940 Arctic Blvd., Ste. 3 Anchorage, AK, 99503		Project Code: 230782 CC: CRW Inc Maria Kampsen		w pertain only to the items tested below. This repo without the prior written approval of Alaska Testlat		
Project:	Lakewood				Man Etanpser		
	Anchorage, AK, 99503 52501.00				laria E Kampsen enior Engineer /25/2023		
Samp	le Details						
	e ID Sample ID ampled		23-0108-S01 BH-04 Sa1	23-0108-S0 BH-04 Sa			
Other	Test Results						
Descri	ption	Method		Results		Limits	
Water C	Content (%)	ASTM D2216	10		0 7		
Date Te	sted		1/18/2023	1/18/202			
Tested I			Tammy Lozano	Tammy Lozar	· · · · · · · · · · · · · · · · · · ·		
Group C		ASTM D2487	GW	G	P		
Group N			Well-graded gravel with sand	Poorly graded gravel with sai			
	g Limits Estimated		Yes	Ye			
Gravel (				-	67		
Sand (%				3	80		
Fines (%	,			Kanan la dua	3		
Tested I	Ву	ASTM D2487	٨	Karen Jackso	n		
Method	tion Mothed	ASTM D6913	A Oven Dry				
•	tion Method site Sieving?		Oven Dry Yes				
	ing Sieve(s)		No. 4				
	ing sieve(s)		31.16				
Cu		ASTM D2487					

ATL	

	erial Test F	-	Issue No: 1				
Client:	CRW Engineering Group 3940 Arctic Blvd., Ste. 3 Anchorage, AK, 99503			The results contained below pertain only to the items tested below. This report should not be reproduced, except in full, without the prior written approval of Alaska Testlab or the agency.			
Project:	Lakewood			MarEtarpser			
	Anchorage, AK, 99503 52501.00			Reviewed By: Maria E Kampsen Title: Senior Engineer Date: 1/25/2023			
Samp	le Details						
Sample ID Client Sample ID Date Sampled		23-0108-S04 BH-04 Sa4	23-0108-S05 BH-04 Sa5	23-0108-S06 BH-04 Sa6			
Other	Test Results						
Descrip		Method		Results		Limits	
Water C Date Te Tested E		ASTM D2216	8 1/18/2023 Tammy Lozano	6 1/18/2023 Tammy Lozano	7 1/18/2023 Tammy Lozano		
Group C Group N	Code lame g Limits Estimated %) 6)	ASTM D2487		Poorly graded gravel with silt and sand Yes 53 42 5			

ATL

Material Tes	st Report		R	eport No: MAT sue No: 1		alaskalesilab.com	
3940 Arctic Blvd., Anchorage, AK, 9 <b>Project:</b> Lakewood	CRW Engineering Group, Inc     Project Code: 230782       3940 Arctic Blvd., Ste. 300     CC: CRW Inc       Anchorage, AK, 99503     Maria Kampsen			The results contained below pertain only to the items tested below. This report should not be reproduced, except in full, without the prior written approval of Alaska Testlab or the agency.			
Anchorage, AK, 9 52501.00	9503		Tit	eviewed By: Maria tle: Senior ate: 1/25/2	r Engineer		
Sample Details		Particle Size Distribution					
Sample ID Client Sample ID	23-0108-S01 BH-04 Sa1			Method: Drying By:	ASTM D6913 Oven 1/20/2023 Karen Jackson		
				Sieve Size 3in 2in 1½in 1in ¾in ½in	<b>% Passing</b> 100 100 100 90 78 56	Limits	
Other Test Result	S			3/8in	48		
Description Water Content (%) Date Tested Tested By	Method ASTM D2216 Tam	Result 10 1/18/2023 my Lozano	Limits	No.4 No.10 No.20 No.40	36.8 28 19 10		
Group Code Group Name Atterberg Limits Estimate Method	ASTM D2487 Well-graded grave ed ASTM D6913	GW I with sand Yes A		No.60 No.100 No.200	6 5 4		
Preparation Method Composite Sieving? Separating Sieve(s) Cu Cc Date Tested	ASTM D2487	Oven Dry Yes No. 4 31.16 1.07 1/20/2023		_			
				Chart			
				Chart			
				100 60 100 (see 30 (see 30 (see 30 (see 30 (see 31 (s		00 200 100 50 µm	

### Comments

Soil Classification of Fines (-#200) in Sieve Analyses Assumed Unless Verified by Additional Testing No Plasticity Index Test Performed